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ANFIS Parallelization Control on Triple-Axis Sun Tracker to Minimize Solar Rays Incidence Angle on Photovoltaic

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ABSTRACT This study proposes an Adaptive Neuro-Fuzzy Inference System (ANFIS) based on model with parallelization control techniques implemented in a triple-axis sun tracker system. The system aims to maximize solar energy absorption by minimizing the angle of incidence of sunlight on Photovoltaic (PV) panels. It is designed with three manipulator arms, each controlled in parallel by a distinct ANFIS model. The primary goal is to adjust the PV panel orientation to optimal azimuth and altitude angles. A tetrahedron sensor is employed to detect the direction of sunlight. This study tests various types of consequent rules to find the optimal configuration for each ANFIS model, including first-order, second-order, and third-order polynomial functions. The analysis results show that the second-order consequent rule provides the highest accuracy across the three ANFIS models. The proposed system can cover an azimuth range from 0° to 360° and an altitude angle from 60° to 90°. It also demonstrates a fast response with a rise time of 1.34 seconds and an angular velocity of 37.3 deg/s. These findings indicate that ANFIS with parallelization control techniques can minimize the angle of sunlight incidence, enhance system flexibility, and accelerate response time, making it a viable solution for increasing energy harvesting by PV panels.

INDEX TERMS ANFIS, parallelization control, photovoltaic, sun tracker, triple-axis

I. INTRODUCTION

The sun tracker system is designed to automatically follow the sun's movement, maximizing sunlight reception on Photovoltaic (PV) panels [1]. This technology is essential in increasing energy production in PV systems, especially in areas with high sunlight intensity. PV efficiency heavily depends on the angle of sunlight incidence on the PV surface. The more optimal the angle, the greater the amount of sunlight absorbed, increasing the electrical energy produced [2], [3]. To maximize generated energy, the orientation of the panels needs to be adjusted in real-time so that the PV always maintains an optimal angle to the sunlight [4]–[6]. Conventional solar power plants are generally installed statically, so PV panels do not receive optimal sunlight exposure, especially in the morning and evening [7], [8]. A sun tracker system can dynamically

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adjusted the PV orientation to remain perpendicular to the sunlight, thereby maximizing the electrical energy obtained [9]–[11]. Sun tracker systems have been discussed in several studies, including in [12], where a comparison between fixed PV systems and sun trackers was conducted. The results showed that sun trackers can increase electricity generation by 30% compared to fixed PV systems. Another study in [13] examined a sun tracker system using a Stewart platform mechanism, demonstrating that the sun tracker system can enhance energy generation by 32% compared to fixed PV systems. Additionally, [14] compares energy produced and consumed by sun tracker systems. The findings indicate that the total energy obtained from a sun tracker system is 26.9% higher than from a fixed PV system, with the energy consumption of the sun tracker reaching 5.63% or around 21.22 Wh and total energy production of 376.85 Wh. These studies show that sun trackers are superior to fixed PV systems. Furthermore, as discussed in [15], the popularity of sun tracker systems continues to rise along with the growing use of solar energy as an alternative energy source. Further developments in sun tracker systems cover various aspects, including manual control through internet networks as studied in [16], [17], bluetooth-based control as examined in [18], and automatic control using solar trajectory models as explored in [19], [20].

In its implementation, a sun tracker requires an effective sensor to accurately detect the sun's position coordinates. This study proposes a type of sensor called a tetrahedron sensor. The survey of the tetrahedron sensor was first introduced in [21], which analyzed the design and structure of the sensor, consisting of three photoresistors. The study's results demonstrated that the tetrahedron sensor could detect the sun's position with a maximum wide Field of View (FOV) of 289.4° and an accuracy of $\pm 1.67^{\circ}$. Further research on the tetrahedron sensor is discussed in [22], which focuses on developing a sensor based on phototransistors to replace photoresistors. Additionally, [23] examined the effect of the tetrahedron sensor's dimensions on the sun tracker's performance in tracking the sun's position. The results showed that increasing the height of the tetrahedron correlates with an increase in FOV, where a tetrahedron with a height of 4.5 cm has an FOV of 289.4°, while a height of 10.2 cm reaches an FOV of 310°.

An appropriate control algorithm and drive mechanism are needed to control the orientation movement of a sun tracker. The control algorithm is necessary to quickly and stably adjust the panel position, reducing energy losses caused by suboptimal angles of incidence. Meanwhile, the drive mechanism is required to support smooth and precise movements. Several studies have examined single-axis and dual-axis drive mechanisms with various algorithms, as shown in Table 1. Based on these studies, the design of the control mechanism in a sun tracker significantly influences the system's response time in following the sun's movement. On the other hand, some studies have developed triple-axis drive mechanisms. This mechanism is designed to improve the vertical orientation adjustment of PV panels. In [24], it is stated that the efficiency of commercial PV typically ranges from 10-20%. Applying a triple-axis mechanism to the sun tracker increases PV efficiency by up to 25%. In [25], it is revealed that the power output generated by PV on a triple-axis sun tracker is 19% greater than that of a dual-axis mechanism. This improvement is due to the triple-axis mechanism's ability to adjust the PV panel's height, enabling it to prevent shadows from surrounding objects from falling onto the panel surface. Furthermore, [26] states that a triple-axis sun tracker can be implemented on a mobile platform, allowing the panel to adjust its orientation to maintain an optimal position even if the platform moves. Although triple-axis sun trackers have significant potential for improving PV efficiency, there are still technical challenges in determining a control method to

ANFIS is an algorithm that combines approaches from Artificial Neural Networks (ANN) and Fuzzy Inference Systems (FIS) to model complex relationships between inputs and outputs [28]. FIS handles uncertain data using fuzzy rules and membership functions to map input values into fuzzy sets [29]. Meanwhile, ANN is responsible for the learning process, where parameters within the fuzzy system, such as membership functions and fuzzy rules, are automatically optimized based on the provided training data [30]. The main processes in ANFIS include fuzzification, which transforms input values into fuzzy values; fuzzy inference, which generates fuzzy output based on fuzzy rules; and defuzzification, which converts the fuzzy output into a numerical value [31], [32]. Several studies have explored the application of ANFIS in various fields. For example, in [33], ANFIS was applied to model machine behaviour in a gas turbine by estimating its operational parameters and improving its performance and durability. Furthermore, [34] discusses the application of ANFIS for controlling dynamic force and position in a Programmable Universal Machine for Assembly (PUMA) robot. Another study [35], applied ANFIS to model the behaviour of an air spring system, which was used to control the solenoid valve of the air spring system to reduce mass acceleration. In addition, other studies have discussed the application of ANFIS in controlling sun trackers. For instance, [36] compared the performance of a Proportional Integral Derivative (PID) controller with ANFIS, with both algorithms optimized using the Firefly Algorithm (FA) to enhance system speed and stability. The findings showed that the ANFIS-FA combination significantly reduced overshoot and accelerated settling time. Furthermore, [37] explored the ANFIS application by comparing single-axis and dual-axis sun tracker mechanisms, concluding that ANFIS with five membership functions was more optimal in controlling both sun tracker mechanisms, yielding high prediction accuracy and low error. Additionally, [38] conducted further analysis on ANFIS as a sun tracker controller, examining the effect of the number of membership functions on model training. This study revealed that the number of membership functions directly affects model performance, with an increase in membership functions leading to reduced error. Based on these studies, it is concluded that the ANFIS model can improve control performance in sun tracker systems, especially with additional optimization or increased membership functions. This makes ANFIS a practical approach for controlling PV panel orientation.

Based on these studies, a sun tracker system with a tripleaxis drive mechanism is proposed. This proposed

Paper	Year	Algorithm	Control Mechanism	Rise Time (s)	%Error
Yuwaldi Away et al. [39]	2023	PID-ANN	Dual-Axis	2.18	1.75%
Andri Novandri et al. [40]	2022	PID	Dual-Axis	1.85	2.6%
Fitri Rahmah et al. [41]	2022	Fuzzy-PD	Single-Axis	7.43	0.43%
Baisrum et al. [42]	2021	ANFIS	Single-Axis	-	1.25%
Imam Abadi et al. [43]	2020	Fuzzy-PID	Dual-Axis	8.2	-
Jalal Farazi et al. [44]	2020	PO-ANN	Dual-Axis	0.94	-
Zubairu A. Yusuf et al. [45]	2019	ABC	Single-Axis	2.37	-
Bamigboye O. Oladayo et al. [46]	2016	IMC-PID	Dual-Axis	1.78	-
Mirza Muhammad Sabir et al. [47]	2016	PID	Dual-Axis	2.2	0.5%

TABLE 1. Literature review of control mechanism on sun tracker

mechanism uses three manipulator arms, each driven by a servo motor. These three arms adjust the PV panel orientation along three axes, allowing the sun tracker to control movement at azimuth and altitude angles. A tetrahedron sensor consisting of three phototransistors arranged on each side of the tetrahedron, detects the sun's position. Additional optimization of the ANFIS algorithm is proposed to control the servo motors by applying a parallelization control technique. This control method aims to divide computational processes into parts that can be executed in parallel, thereby enhancing computational efficiency and processing speed, especially in complex tasks. Parallelization control enables multiple control processes to run simultaneously, reducing latency and improving system responsiveness. In this proposed sun tracker, the system is divided into three processes that are responsible for controlling each servo motor's rotation angle. Input data is obtained from the tetrahedron sensor readings, with input variables varying for each process, resulting in distinct ANFIS models. ANFIS modelling is conducted by designing the network structure, determining the membership functions, and establishing fuzzy rules. Within the fuzzy rules is a consequent rule, part of the fuzzy rule that defines the output based on the fulfilled input conditions. An analysis of the consequent rules is necessary to achieve an optimal model. This study examines three types of consequent rules to identify the most optimal model. The three types of proposed consequent rules are polynomial functions of first-order, second-order, and thirdorder. Each of these orders has different complexity and mapping capabilities in identifying the relationship between inputs and outputs, requiring evaluation to determine the most suitable model for the sun tracker. The main contributions of this paper are as follows:

- We propose a triple-axis mechanism to control the sun tracker using a drive system consisting of three manipulator arms, each driven by a servo motor. The movement of each arm can affect the azimuth and altitude angles of the sun tracker, allowing it to adjust the angle of incoming sunlight on the PV panel surface.
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- We propose an ANFIS algorithm with a parallelization control technique to control the movement of the three servo motors through separate control processes. The system is divided into three processes, each using a different model. This technique can improve computational speed and overall system responsiveness.
- We analyze three types of ANFIS consequent rules, first-order, second-order, and third-order polynomial equations, to determine the most optimal consequent rule for modelling the relationship between input and output variables. This will be enable the sun tracker system to achieve greater precision in following the sun's movement.

II. MATERIAL AND METHODS

A. TETRAHEDRON SENSOR



FIGURE 1. Tetrahedron sensor

The tetrahedron sensor is a type of sensor used to detect the position of sunlight. This sensor has a pyramid shape with three sides, each equipped with a light sensor in the form of a phototransistor. Figure 1 shows a phototransistor in the center of each side of the pyramid, with each position labelled P_1 , P_2 , and P_3 . The sensor has a height of 10 cm and a base length of 5 cm. The type of light sensor and the dimensions of the tetrahedron are based on previous studies [22], [23]. The

tetrahedron sensor operates on the principle of comparing values from each phototransistor. Based on these comparisons, the sensor can determine the sun's position regarding azimuth and altitude.

B. ADAPTIVE NEURO-FUZZY INFERENCE SYSTEM

ANFIS is a hybrid intelligent system that combines the strengths of fuzzy logic and ANN. Fuzzy logic provides a reasoning approach that mimics human thinking and can handle uncertainty and ambiguity. At the same time, ANN can learn from data and recognize complex patterns [48], [49]. The ANFIS architecture consists of several layers, each responsible for specific operations. The first layer performs fuzzification, where membership functions map input values to fuzzy sets. The second layer is the rule layer, where the firing strength of fuzzy rules is calculated. The third layer normalizes the firing strengths, while the fourth layer generates the output by multiplying the normalized firing strength with the consequent part of the fuzzy rules. Finally, the output layer combines these results to produce the final output [50].



FIGURE 2. The architecture of ANFIS network

ANFIS is trained to optimize fuzzy parameters through a learning method that combines the concepts of ANN and fuzzy. The training starts by determining the initial structure of ANFIS, including fuzzy rules, membership functions, and rule types [51]. Training data guides the training process, where the system updates the membership function and consequent parameters [52]. The training process typically consists of two phases: forward pass and backward pass. In the first process, the forward pass, input is fed into ANFIS, and the output is computed through the fuzzy inference mechanism, including fuzzification, firing strength calculation, normalization, and defuzzification to produce the final output [53]. The proposed ANFIS network structure in this study is shown in Figure 2. The first layer is the fuzzification layer, where each node in this layer calculates the membership degree of each input based on the corresponding membership function. The membership function of each input can be calculated using the following equation [54],

$$\mu_j(x_i) = f_j(x_i) \tag{1}$$

where, $\mu_j(x_i)$ is the membership degree for input x_i in the fuzzy set *j* and $f_j(x_i)$ is the membership function of input x_i in the fuzzy set *j*. In this study, a Gaussian Membership Function is used, which is expressed in the following equation,

$$f(x) = gaussian(x; c, \sigma) = e^{-\frac{1}{2}\left(\frac{x-c}{\sigma}\right)^2}$$
(2)

where, *c* is the mean value that serves as the center of the membership function, and σ is the standard deviation that determines the width of the membership function.

The second layer is the rule layer, where each node represents the firing strength for each fuzzy rule formed based on the combination of membership functions for each input. The firing strength is calculated as the product of the input signals that represent the premises in the fuzzy rules, as expressed in the following equation,

$$w_i = \prod_{i=1}^{3} \mu_j(x_i)$$
 (3)

where, w_i represents the output firing strength for rule *i*. Then, the firing strength values are normalized in the third layer, the normalization layer. This process ensures that the relative contribution of each fuzzy rule is correctly accounted for so that the total firing strength of all rules equals 1. The normalization process is performed using the following equation,

$$\overline{w_i} = \frac{w_i}{\sum_{i=1}^N w_i} \tag{4}$$

where, $\overline{w_i}$ represents the normalized firing strength and *N* is the number of fuzzy rules. Next, in the fourth layer, the defuzzification layer, each node multiplies the normalized firing strength by the output of the consequent fuzzy rule using the following equation,

$$z_i = \overline{w_i} \,.\, f(x_i) \tag{5}$$

where, z_i represents the defuzzified output for input x_i and $f(x_i)$ represents the output of the consequent rule for rule *i*. The consequent rule is a mathematical expression that determines the fuzzy output based on the input and the existing rules.

Next, in the fifth layer is the output layer. In this layer, each node combines all the signals received from the previous layers to produce the final output of the ANFIS, as expressed by the following equation,

$$y = \sum_{i=1}^{N} z_i \tag{6}$$



The consequent parameters are updated using the Least Squares Estimation (LSE) method by calculating the error between the system output y and the target output y_t , based on the total dataset m. The error is defined as follows,

$$E = \frac{1}{2} \sum_{i=1}^{m} (y_i - y_{t,i})^2$$
(7)

After that, in the second process, the backward pass is performed using the backpropagation method to minimize the error by updating the parameters c and σ of the membership function based on the calculated error. To update the parameter c, the following equation is used,

$$c_{new} = c_{old} - \eta \frac{\partial E}{\partial c} \tag{8}$$

where, $\frac{\partial E}{\partial c}$ is the partial derivative of the error concerning *c* and η is the learning rate. Then, to update the parameter σ , the following equation is used,

$$\sigma_{new} = \sigma_{old} - \eta \, \frac{\partial E}{\partial \sigma} \tag{9}$$

where, $\frac{\partial E}{\partial \sigma}$ is the partial derivative of the error concerning σ . This process is repeated until the error reaches a minimum value or until a certain number of iterations is reached.



FIGURE 3. Proposed triple-axis sun tracker

C. SUN TRACKER SYSTEM

Figure 3 shows the physical device of the sun tracker system. The proposed design implements a triple-axis mechanism with three manipulator arms. This mechanism allows the system to follow the sun's position more quickly as the motors move in parallel. The system uses servo motors as its actuators.



FIGURE 4. The movement of sun's position

In the testing process, the sun tracker system is compared with the sun's movement path to evaluate the performance of the proposed system. Figure 5 illustrates the position of the sun relative to the tracker. Two main parameters are used to determine the sun's position: azimuth and altitude. Azimuth is the horizontal angle measured clockwise from the north. An angle of 90° means the sun is in the east, 180° in the south, and 270° in the west. Azimuth indicates the sun's direction along the horizon [55]. Meanwhile, altitude measures the sun's height above the horizon, calculated from the horizontal line to the sun's position. This angle changes throughout the day, starting at 0° when the sun rises, reaching its peak at noon, and then returning to 0° when the sun sets [56]. The sun's movement path can be calculated using astronomical formulas based on location and time. The equation to calculate the solar azimuth angle (ϕ_s) is expressed as follows,

$$\sin \phi_S = \frac{\cos \delta \, . \sin \gamma_H}{\cos \varphi_S} \tag{10}$$

where, δ is the solar declination angle, which can be calculated using the following equation,

$$\delta = 23.45^{\circ} . \sin\left(360 . \frac{284 + n}{365}\right) \tag{11}$$

where, *n* is the day number in the year. Meanwhile, γ_H is the solar hour angle, expressed as follows,

$$\gamma_H = 15^{\circ} \left(T_r - 12 \right) \tag{12}$$

where, T_r is the true time, ranging from 0 to 24 hours. Then, φ_S is the solar altitude angle, expressed as follows,

$$\sin \varphi_{\rm S} = \sin \omega \, . \, \sin \delta + \cos \omega \, . \, \cos \delta \, . \, \cos \gamma_{\rm H} \tag{13}$$

where, ω represents the latitude coordinate based on the location on earth.





FIGURE 5. Block diagram of proposed tracker system with ANFIS parallelization control

III. PROPOSED METHOD

The proposed method includes ANFIS modelling and determining the most optimal consequent rule to be applied. It also explains the proposed mechanical structure in the solar tracking system, which aims to optimize the movement of the solar panels to enhance solar energy absorption efficiency.

TABLE 2.	Proposed	ANFIS	structure
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Parameter	Value	Description
Number of input	3	Number of nodes in the input layer
Number of output	1	Number of nodes in the output layer
Number of fuzzy MF 1	3	Number of membership functions at input node 1
Number of fuzzy MF 2	3	Number of membership functions at input node 2
Number of fuzzy MF 3	3	Number of membership functions at input node 3
Membership function	Gaussian function	Membership function at input
Number of rules	27	Number of rules fuzzy
Number of datasets	1945	Number of data for training process
Learning rate	0.01	ANFIS learning rate parameter

A. ANFIS MODEL

In this study, ANFIS is used to control the movement of servo motors based on the light intensity readings from the tetrahedron sensor. The rotation of the motors affects the movement of the manipulator arms, which direct the PV towards the sun. This study proposes ANFIS parallelization control, consisting of three ANFIS models, each responsible for controlling a different motor, as shown in Figure 4, with the structure of each network shown in Table 2. Based on the diagram, ANFIS model 1 controls the angle (θ) of servo motor 1 based on inputs from sensor P_1 , sensor P_2 , and the initial angle (θ_0) of servo motor 1. ANFIS model 2 controls the angle of servo motor 2 based on inputs from sensor P_2 , sensor P_3 , and the initial angle of servo motor 2. Meanwhile, ANFIS model 3 controls the angle of servo motor 3 based on inputs from sensor P_3 , sensor P_1 , and the initial angle of servo motor 3. Then, the forward kinematic method can determine the end-effector points J_1 , J_2 , and J_3 positions. Subsequently, by calculating the normal vector, the azimuth and altitude angles are obtained.

There is a consequent rule in defuzzification, obtaining results based on fuzzy rules by describing the mathematical relationship between input and output [57]. The parameters in the consequent rule are optimized during the training process to ensure that the model can accurately predict the output based on the given data. This paper proposes three types of consequent rules: polynomial functions of firstorder, second-order, and third-order. The first-order function is expressed as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + r$$
(14)

where, $f(x_i)$ represents the output of the consequent rule, p_i is the first-order parameter for input x_i , and r is the bias constant of the rule. Meanwhile, for the second-order function, the equation is as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + \sum_{i=1}^{3} q_i x_i^2 + \sum_{1 \le i < k \le 3} c_{i,k} x_i x_k + r \quad (15)$$

where, q_i is the second-order parameter for input x_i and $c_{i,k}$ is the parameter for the cross terms between inputs x_i and x_k . Then, for the third-order function, the equation is as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + \sum_{\substack{i=1\\3\\i=1}}^{3} q_i x_i^2 + \sum_{\substack{1 \le i < k \le 3\\i \le i < k \le 3}} c_{i,k} x_i x_k + \sum_{\substack{i=1\\i=1}}^{3} t_i x_i^3 + r$$
(16)

where, t_i is the second-order parameter for input x_i .

B. MECHANICAL STRUCTURE OF SUN TRACKER

This sun tracker system configuration uses three manipulator arms, as shown in Figure 6. The model of the manipulator arms is arranged in a parallel configuration, with servo motors as the actuators. These three arms are connected to a triangular plane that serves as the base for the PV. Points J_1 , J_2 , and J_3 connect the plane to the manipulator arms. The height of these points will affect the orientation of the PV in following the sun's movement.



FIGURE 6. Triple-arm manipulator configuration on sun tracker system



FIGURE 7. The configuration of arm manipulator: (a) arm structure design, (b) system mechanism

The configuration of the manipulator arm is shown in Figure 7(a). The arm consists of the upper arm (b_i) and the lower arm (a_i) , with lengths of 3.7 cm and 1.6 cm, respectively. Additionally, there are two connection points: the elbow point (E_i) and the end-effector point (J_i) , as well as a drive point M_i as the motor (for i = 1,2,3). The E_i point is the connection between the lower and upper arm, while J_i is

the connection between the upper arm and the base plane where the PV is mounted. Figure 7(b) shows the drive mechanism of the manipulator arm. The angle β_i is the orientation angle of the manipulator arm relative to the *x*-axis. The movement of motor M_i will create an angle θ_i . This angle will affect the value of angle α_i at point E_i , causing the coordinates at point J_i to change. These coordinate changes can be calculated using the following forward kinematic equation [58], [59],

$$\begin{bmatrix} J_i x \\ J_i y \\ J_i z \end{bmatrix} = \begin{bmatrix} (a_i \cdot \cos \theta_i + b_i \cdot \cos(\theta_i + \alpha_i)) \cos \beta_i + M_i x \\ (a_i \cdot \cos \theta_i + b_i \cdot \cos(\theta_i + \alpha_i)) \sin \beta_i + M_i y \\ a_i \cdot \sin \theta_i + b_i \cdot \sin(\theta_i + \alpha_i) + M_i z \end{bmatrix} (17)$$

In this condition, the arm b_i remains perpendicular at 90° to the base, even when motor M_i moves. This is because point J_i is connected to the triangular plane above it, keeping arm b_i perpendicular. The simulation of this movement is shown in Figure 8. Based on this condition, the angle $\alpha_i = 90 + \theta_i$, so by applying the rules $cos(90 + \theta_1) = -sin \theta_i$ and $sin(90 + \theta_1) = cos \theta_i$, the following equation is obtained,

$$\begin{bmatrix} J_i x \\ J_i y \\ J_i z \end{bmatrix} = \begin{bmatrix} (a_i \cdot \cos \theta_i - b_i \cdot \sin 2\theta_i) \cos \beta_i + M_i x \\ (a_i \cdot \cos \theta_i - b_i \cdot \sin 2\theta_i) \sin \beta_i + M_i y \\ a_i \cdot \sin \theta_i + b_i \cdot \cos 2\theta_i + M_i z \end{bmatrix}$$
(18)

In the proposed system, the angle β_i varies for each motor. In Figure 9(a), the top view shows the orientation of motors M_1 , M_2 , and M_3 , each connected to arms a_1 , a_2 , and a_3 at points E_1 , E_2 , and E_3 . The angle between each motor is depicted, with 315° for M_1 , 45° for M_2 , and 180° for M_3 . Meanwhile, Figure 9(b) shows the physical layout or placement positions of the motors and the manipulator arms connected at the same points. These motors are strategically positioned to move each arm accurately.



FIGURE 8. Principle work of manipulator arm movement: (a) downward movement, (b) upward movement



FIGURE 9. The arrangement of servo motors from a top view: (a) orientation of each motor, (b) position of each motor



FIGURE 10. The normal vector on the triangular plane

Next, the tracker system's azimuth and altitude direction are calculated based on each motor's movement angle. To determine these values, it is necessary to calculate the normal vector of the triangular plane, as shown in Figure 10, where $\vec{v_0}$ is the initial normal vector when its direction is perpendicular upward, and \vec{v} is the normal vector when its direction changes. Based on the coordinate points $J_1(x_1, y_1, z_1)$, $J_2(x_2, y_2, z_2)$, and $J_3(x_3, y_3, z_3)$, the normal vector is calculated using the following equation,

$$\vec{v} = \overrightarrow{J_1 J_2} \cdot \overrightarrow{J_1 J_3} \tag{19}$$

where, $\overline{J_1J_2}$ is the vector from point J_1 to point J_2 and $\overline{J_1J_3}$ is the vector from point J_1 to point J_3 . These vectors can be calculated using the following equations,

$$\overrightarrow{J_1J_2} = (x_2 - x_1, y_2 - y_1, z_2 - z_1)$$
(20)

$$\overrightarrow{J_1J_3} = (x_3 - x_1, y_3 - y_1, z_3 - z_1)$$
(21)

Thus, the equation for the normal vector is expressed as follows,

$$\vec{v} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ x_2 - x_1 & y_2 - y_1 & z_2 - z_1 \\ x_3 - x_1 & y_3 - y_1 & z_3 - z_1 \end{vmatrix}$$
(22)

Meanwhile, point G is the centroid of the triangle and can be calculated using the following equation,

$$\begin{bmatrix} G_x \\ G_y \\ G_z \end{bmatrix} = \begin{bmatrix} (x_1 + x_2 + x_3)/3 \\ (y_1 + y_2 + y_3)/3 \\ (z_1 + z_2 + z_3)/3 \end{bmatrix}$$
(23)

Based on the normal vector $\vec{v} = (v_x, v_y, v_z)$ obtained, the tilt angle of the plane concerning the *x*-axis (θ_x) and the *y*-axis (θ_x) can be determined using the following equations,

$$\theta_x = \cos^{-1} \left(\frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}} \right)$$
(24)

$$\theta_{y} = \cos^{-1} \left(\frac{v_{y}}{\sqrt{v_{x}^{2} + v_{y}^{2} + v_{z}^{2}}} \right)$$
(25)

Meanwhile, to calculate the tracker azimuth (ϕ_T) and tracker altitude (φ_T), the following equations are used,

$$\phi_T = \tan^{-1} \left(\frac{v_y}{v_x} \right) \tag{26}$$

$$\varphi_T = \tan^{-1} \left(\frac{v_z}{\sqrt{v_x^2 + v_y^2}} \right) \tag{27}$$

IV. PERFORMANCE ANALYSIS

The analysis provides performance results of each model in predicting PV output power based on its operational temperature. The analytical methods used include calculating Mean Absolute Error (MAE), Root Mean Squared Error (RMSE), Mean Absolute Percentage Error (MAPE), Coefficient of Determination (R^2), and Coefficient of Variation (CoV).

MAE is one of the commonly used methods to analyze model performance. It measures the average absolute difference between the predicted values generated by the model and the actual values in the test data. This result shows how closely the model predictions match the actual values overall. The equation for MAE is as follows,

$$MAE = \frac{1}{n} \sum_{i=n}^{n} |y_i - \hat{y}_i|$$
(28)

where, *n* is the number of test data points, y_i is the actual value, and \hat{y}_i is the value predicted by the model for the *i* data point. A lower MAE value indicates better model performance, signifying that the model's predictions are closer to the actual values [60]. Next, RMSE analysis is conducted by calculating the square root of the average of the squared differences between the model's predicted values and the actual values. The equation for RMSE is defined as follows,

Madal	Parameter	Baramatan Training			Testing			
wiodei		First-Order	Second-Order	Third-Order	First-Order	Second-Order	Third-Order	
	MAE	9.3	3.6	5.26	9.57	2.82	4.08	
	RMSE	11.61	4.5	6.21	11.33	3.34	4.95	
ANFIS 1	MAPE	21.79%	8.08%	17.08%	21.78%	7.02%	10.5%	
	\mathbb{R}^2	0.81	0.98	0.96	0.83	0.99	0.97	
	CoV	0.39	0.49	0.47	0.42	0.47	0.44	
	MAE	11.09	3.82	5.08	9.79	3	3.51	
	RMSE	13.78	4.74	6.05	11.81	3.58	4.33	
ANFIS 2	MAPE	19.44%	8.3%	12.86%	21.57%	6.44%	8.79%	
	\mathbb{R}^2	0.69	0.97	0.95	0.82	0.99	0.98	
	CoV	0.3	0.42	0.4	0.4	0.46	0.46	
	MAE	11.76	3.8	4.41	8.94	2.86	2.77	
	RMSE	14.1	4.68	5.33	10.86	3.48	3.4	
ANFIS 3	MAPE	22.83%	7.69%	8.83%	18.52%	6.35%	6.11%	
	R ²	0.7	0.98	0.97	0.85	0.99	0.99	
	CoV	0.35	0.48	0.43	0.41	0.47	0.47	

TABLE 3. The results of ANFIS training and testing with various consequent rules

$$RMSE = \sqrt{\frac{1}{n} \sum_{i=n}^{n} (y_i - \hat{y}_i)^2}$$
(29)

RMSE analysis indicates the average deviation between the model's predicted and actual values. By taking the square root, RMSE offers a more intuitive interpretation in the same units as the target variable. A lower RMSE value indicates better model performance, meaning the model's predictions are closer to the actual values [61]. Next, MAPE analysis is a method to measure the error rate of a model by calculating the average of the absolute percentage error between the predicted and actual values. The equation for calculating MAPE is defined as follows,

$$MAPE = \frac{1}{n} \sum_{i=n}^{n} \left| \frac{y_i - \hat{y}_i}{y_i} \right| .100\%$$
(30)

The MAPE value indicates the prediction error in percentage terms. The lower the MAPE value, the better the model's performance in predicting the data. One advantage of MAPE is its ease of interpretation, as the result is a percentage. Next, the R^2 analysis, known as the Coefficient of Determination, is used to measure how well the developed model can explain the variability in the data. The equation for the Coefficient of Determination is defined as follows,

$$R^{2} = 1 - \frac{\sum_{i=1}^{n} (y_{i} - \hat{y}_{i})^{2}}{\sum_{i=1}^{n} (y_{i} - \hat{y})^{2}}$$
(31)

where, \hat{y} is the mean of all y_i values. The R^2 value ranges from 0 to 1, where a value closer to 1 indicates that the model better explains the variability in the data. R^2 analysis can determine how much output data variability can be explained by the input data. Lastly, the CoV analysis, or Coefficient of Variation, is a statistical measure to assess a dataset's relative degree of variation. CoV is defined as the ratio of the standard deviation to the mean, expressed as follows,

$$CoV = \frac{\sqrt{\frac{1}{n}\sum_{i=1}^{n} \left(y_{i} - \frac{1}{n}\sum_{i=1}^{n} y_{i}\right)^{2}}}{\frac{1}{n}\sum_{i=1}^{n} y_{i}}$$
(32)

CoV is typically used to measure data stability. A low CoV value indicates more stable data, while a high CoV value suggests more significant variability in the data.

V. RESULTS AND DISCUSSION

In this section, an evaluation is conducted to assess the performance of ANFIS in each model based on the type of consequent rule. Then, the movement of the three motors is simulated to obtain the azimuth and altitude angles. Testing uses the sun tracker device to assess the system's ability to track the sun's position. Finally, comparing previous systems is necessary to validate the proposed sun tracker system's effectiveness.

A. MODEL PERFORMANCE ANALYSIS

Table 3 presents the statistical results from the model's training and testing phases based on three types of consequent rules: first-order, second-order, and third-order. The dataset consists of 80% for training and 20% for testing. The ANFIS



training and testing results show that the choice of consequent rule significantly impacts each model's performance.

FIGURE 11. The comparison analysis of consequence rule variations to controlling motor movements (a) ANFIS 1 model, (b) ANFIS 2 model, (c) ANFIS 3 model

In ANFIS model 1, the second-order performed best compared to the first-order and third-order, both in the training and testing phases. During training, the second-order achieved the lowest MAE, RMSE, and MAPE values, at 3.6, 4.5, and 8.08%, respectively, along with a high R^2 value of 0.98. This result indicates that the model can predict motor movement accurately based on the input data. In testing, the second-order also excelled with the lowest MAE, RMSE, and MAPE values, at 2.82, 3.34, and 7.02%, respectively, indicating accurate model performance with minimal error. In ANFIS model 2, a similar pattern emerged, with the secondorder demonstrating optimal performance. During training, the second-order model yielded low MAE, RMSE, and MAPE values of 3.82, 4.74, and 8.3%, along with a high R^2 value of 0.97. In testing, the second-order produced MAE, RMSE, and MAPE values of 3, 3.58, and 6.44%, respectively, outperforming the first-order and third-order models. In ANFIS model 3, the second-order also provided the best results, achieving the lowest error values in training with MAE, RMSE, and MAPE of 3.8, 4.68, and 7.69%, respectively, and the highest R^2 value of 0.98. However, in testing, the second-order's performance was less optimal than the third-order, as indicated by higher MAE, RMSE, and

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MAPE values than the third-order. The training and testing analysis results show that the second-order consequent rule is optimal for all three ANFIS models.

Figure 11(a) displays the motor movement results with different consequent rules. The graph shows that all three consequent rules follow the angle change patterns quite well, although first-order shows more significant discrepancies. Meanwhile, in Figure 11(b), the first-order consequent rule exhibits noticeable differences, especially in the sixth and eighth experiments. On the other hand, second-order and third-order are more consistent in approaching the actual angle, although slight differences still exist at some points. In Figure 11(c), the average difference between the actual angle and the angle produced by each consequent rule is more minor than the previous graph. Overall, although both second-order and third-order consequent rules accurately follow the angle change patterns of all three motors, there are some points where the second-order performs better than the third-order. Figure 12 shows a three-dimensional graph illustrating the relationship between the ratio of two phototransistor values and the output as the motor angle increments for each consequent rule. The comparison values from the two phototransistor readings directly affect the magnitude of the resulting angle increment. In the first-order consequent, the angle increment pattern appears linear. In the second-order consequent, a significant angle increment occurs with more considerable phototransistor ratio differences; the greater the difference, the higher the angle increment. Conversely, there is no considerable angle increase for ratios closer in value. In the third-order, the angle increment pattern is similar to the second-order but displays fluctuations or a nonlinear pattern in the middle of the graph. This indicates that there are points where small changes in the phototransistor ratio can lead to a lower or even decreasing angle increment.







FIGURE 12. The relationship between the phototransistor ratio values with the motor angle increases based on various consequent rules: (a) first-order, (b) second-order, and (c) third-order



FIGURE 13. The simulation of azimuth and altitude changes based on motor movement ($M_1 = 26^\circ, M_2 = 40^\circ, M_3 = -30^\circ$)

After obtaining the model, a motor movement simulation was conducted on the sun tracker to observe the relationship between the movements of the three motors and changes in azimuth and altitude angles. Figure 13 displays the simulation results, showing how each motor's activity influences the panel's orientation changes. In this simulation, it demonstrates the condition where the three motors move at angles $M_1 = 26^\circ$, $M_1 = 40^\circ$, and $M_1 = -30^\circ$, resulting in a normal vector direction of (0, 8, 26) with tilt angles of $\theta_x = 90^\circ$ and $\theta_y = 72^\circ$. Meanwhile, the resulting azimuth and altitude angles are 89° and 72°, respectively. Further testing results are shown in Figure 14, combining an angle range of -30° to 90°, representing the minimum to maximum motor angles. Figure 14(a) shows that the azimuth angle ranges from 0° to 360°, while Figure 14(b) indicates that the altitude angle ranges from 60° to 90°. This angle range demonstrates that the triple-axis mechanism can achieve good orientation flexibility, allowing the system to adjust the PV panel position effectively to minimize the solar incidence angle.



FIGURE 14. The results of the sun tracker movement experiment based on all combinations of angles M_1 , M_2 , and M_3 : (a) azimuth angle movement and (b) altitude angle movement

B. SUN TRACKER SYSTEM PERFORMANCE ANALYSIS Figure 15(a) compares the sun tracker movement and the azimuth angle of the actual sun position. The graph shows the sun tracker accurately follows the sun's azimuth angle from sunrise to sunset. Meanwhile, Figure 15(b) compares the altitude angle. Based on this graph, a discrepancy occurs at the start of tracking, around 7:00 AM to 8:00 AM. Then, the sun tracker successfully tracks the sun's altitude more accurately, reaching a peak at 12:30 PM at its maximum altitude. Afterwards, the altitude of the sun tracker gradually decreases in sync with the sun's position until sunset. Overall, the sun tracker system works effectively to adjust its movement in tracking the sun's position in azimuth and altitude angles, thereby minimizing the solar incidence angle on the PV surface throughout the day.



FIGURE 15. The result comparison between the tracked and the sun's actual position: (a) azimuth movement and (b) altitude movement

Figure 16 shows the rise time graph of the sun tracker system when adjusting the PV panel orientation. The graph reveals that the sun tracker's movement increases exponentially, indicating a reasonably fast response time of approximately 1.34 seconds.



FIGURE 16. The rise time results of the proposed sun tracker system

C. SYSTEM PERFORMANCE COMPARISON

Table 4 compares the proposed ANFIS model's performance with several previous models related to sun tracker systems. The comparison aims to validate the performance of the proposed ANFIS model in tracking the sun's position. The models compared include ANN [4], PID [40], and PID-ANN [39]. The parameters compared are MAE, RMSE, rise time, and speed. Based on the comparison results, the proposed ANFIS model demonstrates the best performance with the lowest MAE and RMSE values, at 1.55 and 2.81, respectively, indicating that this model has the lowest error rate compared to the other models. This model has the fastest rise time of 1.34 seconds, resulting in a speed of 37.3 deg/s. This indicates that the ANFIS parallelization control model is accurate and responsive in following the sun's movement. For comparison, the PID-ANN model recorded an MAE of 1.75, RMSE of 2.61, and a rise time of 2.18 seconds, while the ANN and PID models had MAE values of 1.65 and 2.62, RMSE values of 3.80 and 3.36, and rise times of 2.22 seconds and 2.2 seconds, respectively. The performance of the proposed model shows higher accuracy with lower error and faster system response, making it an effective method for sun tracker system control.

TABLE 4.	The comparison of models	performance
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Model	MAE	RMSE	Rise Time (s)	Speed (deg/s)
ANFIS Parallelization Control (Proposed)	1.55	2.81	1.34	37.3
PID-ANN	1.75	2.61	2.18	21.1
ANN	1.65	3.80	2.22	17.4
PID	2.62	3.36	2.2	20.18

VI. CONCLUSION

Based on the analysis results, all three proposed ANFIS models using the second-order consequent rule deliver the best performance compared to the first-order and third-order, both in the training and testing phases. The simulation results show that the movement of the sun tracker with a triple-axis mechanism can reach an azimuth angle ranging from 0° to 360°. In contrast, the altitude angle ranges from 60° to 90°. These values indicate that the sun tracker has good flexibility. Based on the experimental results of device testing in tracking the sun's position, the sun tracker system achieved low MAE and RMSE values compared to previously studied models, at 1.55 and 2.81, respectively. Regarding responsiveness, the proposed system has a high response speed of 37.3 deg/s, with a rise time of 1.34 seconds, which is faster than other models.

Although the proposed sun tracker system offers improved accuracy and responsiveness in tracking the sun's position, it has some drawbacks, including system complexity, leading to higher energy consumption. This is due to the number of motors that need to move simultaneously to reach the optimal position. The additional energy the motors consume in the triple-axis mechanism can reduce overall energy efficiency, especially in conditions with limited energy sources.

Future research will focus on developing triple-axis sun tracker technology techniques to enhance efficiency by reducing energy consumption and optimizing parallelization control techniques in ANFIS to make it more adaptive in tracking the sun's position.

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Reviewer: 1

The reviewer thinks that the manuscript in its present form is unsuitable for publication in a scientific journal due to the inadequate preparation of the manuscript. In particular, the authors should consider the following remarks and comments in a thoroughly revised version:

The introduction needs to be enhanced. Although authors have incorporated many literatures, the writing stays at a superficial level. It is important to demonstrate the challenge of the research investigated and the gap closed by the proposed work. More explicitly, the novelty and contribution of the proposed work are not well demonstrated.

Also, in the introduction, some credits to the recent works related to the proposed methods are suggested to enrich the literature in the field of control design. More recent research should be mentioned in references (2022-2024). Some related works can be considered, see for example, Integrated Control Design for Hybrid Grid-Photovoltaic Systems in Distillation Applications: A Reference Model and Fuzzy Logic Approach. Control techniques inherently suffer from uncertain disturbances. Referencing to Enhanced wind energy conversion system performance using fast smooth second-order sliding mode control with neuro-fuzzy estimation and variable-gain robust exact output differentiator', discuss in detail about possible mitigation strategies. Also, include results on how much the proposed control law could manage to reduce these disturbances? The equations in the manuscript are not consistently formatted, lack proper explanation, and are not clearly linked to the corresponding discussion, making them difficult to follow and interpret The presentation of the control technique is unclear and lacks sufficient detail. Key concepts are not explained adequately, and the methodology is not illustrated effectively, making it difficult to understand its

implementation and significance.

The comparative analysis is weak. A deeper comparison with other state-of-the-art methods, such as Adaptive FIT-SMC Approach for an Anthropomorphic Manipulator with Robust Exact Differentiator and Neural Network-Based Friction Compensation, would give readers a clearer sense of how the proposed method stands in the broader context of robust control research

The manuscript lacks a detailed discussion on how the various parameters of the proposed controller are selected and tuned. This is highly relevant. So, a more structured approach to tuning these parameters and explaining the trade-offs must be included.

The method's stability is validated using the Lyapunov theory, although this section could benefit from a more thorough discussion. Specifically, the paper could elaborate on the practical implications of the stability guarantees and whether they hold under real-world conditions, particularly under unmodeled dynamics or significant disturbances

The figures lack clarity, proper labeling, and detailed captions, making interpretation difficult. The result discussion is superficial, lacking depth, critical analysis, and comparison with existing literature

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Comments

1. Could the authors explain why ANFIS was chosen for this application over other advanced control approaches like Model Predictive Control or Linear Quadratic Regression?

2. Table 4 compares PID and ANN controllers; could alternative controllers, such as hybrid MPC-ANN systems, provide further insights?

3. How does the computational complexity of the proposed ANFIS parallelisation control compare to the other methods presented, particularly for real-time applications?

4. The text identifies energy consumption as a disadvantage of the triple-axis device. Have the authors researched and tested energy-efficient strategies to address this issue?

5. The second-order consequent rule is identified as optimal. What specific factors contribute to its superior performance compared to the first- and third-order rules in this context?

6. How would the performance of the proposed system vary under partially shaded conditions, and is ANFIS robust enough to handle such scenarios compared to other controllers?

7. The authors focus on minimizing the solar incidence angle; could they elaborate on the practical implications of this in terms of energy efficiency and compare it with systems that prioritize other optimization metrics?

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ANFIS Parallelization Control on Triple-Axis Sun Tracker to Minimize Solar Rays Incidence Angle on Photovoltaic

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ABSTRACT This study proposes an Adaptive Neuro-Fuzzy Inference System (ANFIS) based on model with Parallelization Control Technique (PCT) implemented in a triple-axis sun tracker system. The system aims to maximize solar energy absorption by minimizing the angle of incidence of sunlight on Photovoltaic (PV) panels. It is designed with three manipulator arms, each controlled in parallel by a distinct ANFIS model. The primary goal is to adjust the PV panel orientation to optimal azimuth and altitude angles. A tetrahedron sensor is employed to detect the direction of sunlight. This study tests various types of consequent rules to find the optimal configuration for each ANFIS model, including first-order, second-order, and third-order polynomial functions. The analysis results show that the second-order consequent rule provides the highest accuracy across the three ANFIS models. The proposed system can cover an azimuth range from 0° to 360° and an altitude angle from 60° to 90°. The experiment also demonstrated that the system consistently moves toward a stable condition, even in the presence of minor disturbances. These findings indicate that ANFIS with PCT can minimize the angle of sunlight incidence, enhance system flexibility, and accelerate response time, making it a viable solution for increasing energy harvesting by PV panels.

INDEX TERMS ANFIS, parallelization control, photovoltaic, sun tracker, triple-axis

I. INTRODUCTION

The sun tracker system is designed to automatically follow the sun's movement, maximizing sunlight reception on Photovoltaic (PV) panels [1]. This technology is essential in increasing energy production in PV systems, especially in areas with high sunlight intensity. PV efficiency heavily depends on the angle of sunlight incidence on the PV surface. The more optimal the angle, the greater the amount of sunlight absorbed, increasing the electrical energy produced [2], [3]. To maximize generated energy, the orientation of the panels needs to be adjusted in real-time so that the PV always maintains an optimal angle to the sunlight [4]–[6]. Conventional solar power plants are generally installed statically, so PV panels do not receive optimal sunlight exposure, especially in the morning and evening [7], [8]. A sun tracker system can dynamically adjusted the PV orientation to remain perpendicular to the sunlight, thereby maximizing the electrical energy obtained [9]–[11]. Sun tracker systems have been discussed in several studies, including in [12], where a comparison between fixed PV systems and sun trackers was conducted. The results showed that sun trackers can increase electricity generation by 30% compared to fixed PV systems. Another study in [13] examined a sun tracker system using a Stewart platform mechanism, demonstrating that the sun tracker system can enhance energy generation by 32% compared to fixed PV systems. Additionally, [14] compares energy produced and consumed by sun tracker systems. The findings indicate that the total energy obtained from a sun tracker system is 26.9% higher than from a fixed PV system, with the energy consumption of the sun tracker reaching 5.63% or around 21.22 Wh and total energy production of



376.85 Wh. These studies show that sun trackers are superior to fixed PV systems. Furthermore, as discussed in [15], the popularity of sun tracker systems continues to rise along with the growing use of solar energy as an alternative energy source. Further developments in sun tracker systems cover various aspects, including manual control through internet networks as studied in [16], [17], bluetooth-based control as examined in [18], and automatic control using solar trajectory models as explored in [19], [20].

In its implementation, a sun tracker requires an effective sensor to accurately detect the sun's position coordinates. This study proposes a type of sensor called a tetrahedron sensor. The survey of the tetrahedron sensor was first introduced in [21], which analyzed the design and structure of the sensor, consisting of three photoresistors. The study's results demonstrated that the tetrahedron sensor could detect the sun's position with a maximum wide Field of View (FOV) of 289.4° and an accuracy of $\pm 1.67^{\circ}$. Further research on the tetrahedron sensor is discussed in [22], which focuses on developing a sensor based on phototransistors to replace photoresistors. Additionally, [23] examined the effect of the tetrahedron sensor's dimensions on the sun tracker's performance in tracking the sun's position. The results showed that increasing the height of the tetrahedron correlates with an increase in FOV, where a tetrahedron with a height of 4.5 cm has an FOV of 289.4°, while a height of 10.2 cm reaches an FOV of 310°.

An appropriate control algorithm and drive mechanism are needed to control the orientation movement of a sun tracker. The control algorithm is necessary to quickly and stably adjust the panel position, reducing energy losses caused by suboptimal angles of incidence. Meanwhile, the drive mechanism is required to support smooth and precise movements. Several studies have examined single-axis and dual-axis drive mechanisms with various algorithms, as shown in Table 1. Based on these studies, the design of the control mechanism in a sun tracker significantly influences the system's response time in following the sun's movement. On the other hand, some studies have developed triple-axis drive mechanisms. This mechanism is designed to improve the vertical orientation adjustment of PV panels. In [24], it is stated that the efficiency of commercial PV typically ranges from 10-20%. Applying a triple-axis mechanism to the sun tracker increases PV efficiency by up to 25%. In [25], it is revealed that the power output generated by PV on a triple-axis sun tracker is 19% greater than that of a dual-axis mechanism. This improvement is due to the triple-axis mechanism's ability to adjust the PV panel's height, enabling it to prevent shadows from surrounding objects from falling onto the panel surface. Furthermore, [26] states that a triple-axis sun tracker can be implemented on a mobile platform, allowing the panel to adjust its orientation to maintain an optimal position even if the platform moves. Although triple-axis sun trackers have significant potential for improving PV efficiency, there are still technical challenges in determining a control method to

optimize panel orientation. With the proper control method, the system can adapt to changes in the sun's position and avoid shadows from objects falling on the panel surface [27]. One approach capable of adapting to changing conditions is the Adaptive Neuro-Fuzzy Inference System (ANFIS).

ANFIS is an algorithm that combines approaches from Artificial Neural Networks (ANN) and Fuzzy Inference Systems (FIS) to model complex relationships between inputs and outputs [28]. FIS handles uncertain data using fuzzy rules and membership functions to map input values into fuzzy sets [29]. Meanwhile, ANN is responsible for the learning process, where parameters within the fuzzy system, such as membership functions and fuzzy rules, are automatically optimized based on the provided training data [30]. The main processes in ANFIS include fuzzification, which transforms input values into fuzzy values; fuzzy inference, which generates fuzzy output based on fuzzy rules; and defuzzification, which converts the fuzzy output into a numerical value [31], [32]. Several studies have explored the application of ANFIS in various fields. For example, in [33], ANFIS was applied to model machine behaviour in a gas turbine by estimating its operational parameters and improving its performance and durability. Furthermore, [34] discusses the application of ANFIS for controlling dynamic force and position in a Programmable Universal Machine for Assembly (PUMA) robot. Another study [35], applied ANFIS to model the behaviour of an air spring system, which was used to control the solenoid valve of the air spring system to reduce mass acceleration. In addition, other studies have discussed the application of ANFIS in controlling sun trackers. For instance, [36] compared the performance of a Proportional Integral Derivative (PID) controller with ANFIS, with both algorithms optimized using the Firefly Algorithm (FA) to enhance system speed and stability. The findings showed that the ANFIS-FA combination significantly reduced overshoot and accelerated settling time. Furthermore, [37] explored the ANFIS application by comparing single-axis and dual-axis sun tracker mechanisms, concluding that ANFIS with five membership functions was more optimal in controlling both sun tracker mechanisms, yielding high prediction accuracy and low error. Additionally, [38] conducted further analysis on ANFIS as a sun tracker controller, examining the effect of the number of membership functions on model training. This study revealed that the number of membership functions directly affects model performance, with an increase in membership functions leading to reduced error. Moreover, ANFIS offers the flexibility of fuzzy logic, enabling it to learn from data automatically adjust and parameters [39]. The implementation of ANFIS is less complex compared to other control methods, such as Linear Quadratic Regression (LQR) and Model Predictive Control (MPC). MPC has significantly higher complexity than ANFIS, as it requires solving optimization problems at each time step to



Paper	Year	Algorithm	Control Mechanism	Rise Time (s)	%Error
Yuwaldi Away et al. [44]	2023	PID-ANN	Dual-Axis	2.18	1.75%
Andri Novandri et al. [45]	2022	PID	Dual-Axis	1.85	2.6%
Fitri Rahmah et al. [46]	2022	Fuzzy-PD	Single-Axis	7.43	0.43%
Baisrum et al. [47]	2021	ANFIS	Single-Axis	-	1.25%
Imam Abadi et al. [48]	2020	Fuzzy-PID	Dual-Axis	8.2	-
Jalal Farazi et al. [49]	2020	PO-ANN	Dual-Axis	0.94	-
Zubairu A. Yusuf et al. [50]	2019	ABC	Single-Axis	2.37	-
Bamigboye O. Oladayo et al. [51]	2016	IMC-PID	Dual-Axis	1.78	-
Mirza Muhammad Sabir et al. [52]	2016	PID	Dual-Axis	2.2	0.5%

TABLE 1. Literature review of control mechanism on sun tracker

determine the optimal control signal [40]. Additionally, LQR has low complexity because it only requires solving a functional quadratic equation. However, LQR is not designed to handle nonlinear systems, such as a triple-axis sun tracker [41]. Meanwhile, the ANFIS approach, which is a hybrid algorithm combining ANN and FIS, can quickly adjust parameters. This makes it highly suitable for real-time systems that demand quick responses and the ability to maintain responsiveness to environmental changes [42], [43]. Based on these studies, it is concluded that the ANFIS model can improve control performance in sun tracker systems, especially with additional optimization or increased membership functions. This makes ANFIS a practical approach for controlling PV panel orientation.

Based on these studies, most current sun tracker systems still rely on single-axis or dual-axis mechanisms, which have limitations in vertical adjustments and in avoiding shadows from objects surrounding the panels. On the other hand, research on triple-axis mechanisms is still minimal. Additionally, optimization techniques are needed to enhance the performance of the ANFIS algorithm in managing the complexity of sun tracker systems, particularly in triple-axis mechanisms. As a solution, the sun tracker system with a triple-axis drive mechanism is proposed. This proposed mechanism uses three manipulator arms, each driven by a servo motor. These three arms adjust the PV panel orientation along three axes, allowing the sun tracker to control movement at azimuth and altitude angles. A tetrahedron sensor consisting of three phototransistors arranged on each side of the tetrahedron, detects the sun's position. Additional optimization of the ANFIS algorithm is proposed to control the servo motors by applying the Parallelization Control Technique (PCT). This control method aims to divide computational processes into parts that can be executed in parallel, thereby enhancing computational efficiency and processing speed, especially in complex tasks. PCT enables multiple control processes to run simultaneously, reducing latency and improving system responsiveness. ANFIS-PCT offers an optimal balance between computational complexity, robustness against nonlinearity, and real-time responsiveness, making it the

best solution for triple-axis sun tracker systems. In this proposed sun tracker, the system is divided into three processes that are responsible for controlling each servo motor's rotation angle. Input data is obtained from the tetrahedron sensor readings, with input variables varying for each process, resulting in distinct ANFIS models. ANFIS modelling is conducted by designing the network structure, determining the membership functions, and establishing fuzzy rules. Within the fuzzy rules is a consequent rule, part of the fuzzy rule that defines the output based on the fulfilled input conditions. An analysis of the consequent rules is necessary to achieve an optimal model. This study examines three types of consequent rules to identify the most optimal model. The three types of proposed consequent rules are polynomial functions of first-order, second-order, and thirdorder. Each of these orders has different complexity and mapping capabilities in identifying the relationship between inputs and outputs, requiring evaluation to determine the most suitable model for the sun tracker. This research focuses on minimizing the solar incidence angle to enhance the electrical energy production of PV systems. When the solar incidence angle on the panel surface approaches zero, the amount of sunlight absorbed by the PV reaches its maximum, directly increasing the generated electrical output.

The novelty of this research lies in the implementation of PCT in ANFIS, which enables the division of computational processes into multiple parts running concurrently. Additionally, this study analyzes various consequent rule configurations in the ANFIS model, including first-order, second-order, and third-order polynomial functions, to determine the most optimal configuration. The main contributions of this paper are as follows:

- We propose a sun tracker system using a triple-axis mechanism consisting of three manipulator arms to control the azimuth and altitude angles. This system enables PV panels to adjust their angles optimally to the direction of incoming sunlight.
- We propose an ANFIS algorithm with PCT to control the movement of the sun tracker through separate



control processes, making the system more responsive and accurate.

• We demonstrate that the second-order consequent rule provides the best performance in controlling the sun tracker, effectively minimizing the angle of incoming sunlight on the PV panel.

For convenience, the abbreviations used in this paper are summarized in Table 2.

TABLE 2. Summary of abbreviations

Abbreviation	Meaning
ANFIS	Adaptive Neuro-Fuzzy Inference System
ANN	Artificial Neural Networks
CV	Coefficient of Variation
FIS	Fuzzy Inference Systems
LSE	Least Squares Estimation
MAE	Mean Absolute Error
MAPE	Mean Absolute Percentage Error
PCT	Parallelization Control Technique
PID	Proportional Integral Derivative
PV	Photovoltaic
RMSE	Root Mean Squared Error

II. MATERIAL AND METHODS

A. TETRAHEDRON SENSOR



FIGURE 1. Tetrahedron sensor

The tetrahedron sensor is a type of sensor used to detect the position of sunlight. This sensor has a pyramid shape with three sides, each equipped with a light sensor in the form of a phototransistor. Figure 1 shows a phototransistor in the center of each side of the pyramid, with each position labelled P_1 , P_2 , and P_3 . The sensor has a height of 10 cm and a base length of 5 cm. The type of light sensor and the dimensions of the tetrahedron are based on previous studies [22], [23]. The tetrahedron sensor operates on the principle of comparing values from each phototransistor. Based on these comparisons, the sensor can determine the sun's position regarding azimuth and altitude.

ANFIS is a hybrid intelligent system that combines the strengths of fuzzy logic and ANN. Fuzzy logic provides a reasoning approach that mimics human thinking and can handle uncertainty and ambiguity. At the same time, ANN can learn from data and recognize complex patterns [53], [54]. The ANFIS architecture consists of several layers, each responsible for specific operations. The first layer performs fuzzification, where membership functions map input values to fuzzy sets. The second layer is the rule layer, where the firing strength of fuzzy rules is calculated. The third layer normalizes the firing strengths, while the fourth layer generates the output by multiplying the normalized firing strength with the consequent part of the fuzzy rules. Finally, the output layer combines these results to produce the final output [55].



FIGURE 2. The architecture of ANFIS network

ANFIS is trained to optimize fuzzy parameters through a learning method that combines the concepts of ANN and fuzzy. The training starts by determining the initial structure of ANFIS, including fuzzy rules, membership functions, and rule types [56]. Training data guides the training process, where the system updates the membership function and consequent parameters [57]. The training process typically consists of two phases: forward pass and backward pass. In the first process, the forward pass, input is fed into ANFIS, and the output is computed through the fuzzy inference mechanism. including fuzzification, firing strength calculation, normalization, and defuzzification to produce the final output [58]. The proposed ANFIS network structure in this study is shown in Figure 2. The first layer is the fuzzification layer, where each node in this layer calculates the membership degree of each input based on the corresponding membership function. The membership function of each input can be calculated using the following equation [59],

$$\mu_j(x_i) = f_j(x_i) \tag{1}$$

where, $\mu_j(x_i)$ is the membership degree for input x_i in the fuzzy set *j* and $f_i(x_i)$ is the membership function of input x_i


in the fuzzy set j. In this study, a Gaussian Membership Function is used, which is expressed in the following equation,

$$f(x) = gaussian(x; c, \sigma) = e^{-\frac{1}{2}\left(\frac{x-c}{\sigma}\right)^2}$$
(2)

where, *c* is the mean value that serves as the center of the membership function, and σ is the standard deviation that determines the width of the membership function.

The second layer is the rule layer, where each node represents the firing strength for each fuzzy rule formed based on the combination of membership functions for each input. The firing strength is calculated as the product of the input signals that represent the premises in the fuzzy rules, as expressed in the following equation,

$$w_i = \prod_{i=1}^{3} \mu_j(x_i)$$
 (3)

where, w_i represents the output firing strength for rule *i*. Then, the firing strength values are normalized in the third layer, the normalization layer. This process ensures that the relative contribution of each fuzzy rule is correctly accounted for so that the total firing strength of all rules equals 1. The normalization process is performed using the following equation,

$$\overline{w_i} = \frac{w_i}{\sum_{i=1}^N w_i} \tag{4}$$

where, $\overline{w_i}$ represents the normalized firing strength and *N* is the number of fuzzy rules. Next, in the fourth layer, the defuzzification layer, each node multiplies the normalized firing strength by the output of the consequent fuzzy rule using the following equation,

$$z_i = \overline{w_i} \,.\, f(x_i) \tag{5}$$

where, z_i represents the defuzzified output for input x_i and $f(x_i)$ represents the output of the consequent rule for rule *i*. The consequent rule is a mathematical expression that determines the fuzzy output based on the input and the existing rules.

Next, in the fifth layer is the output layer. In this layer, each node combines all the signals received from the previous layers to produce the final output of the ANFIS, as expressed by the following equation,

$$y = \sum_{i=1}^{N} z_i \tag{6}$$

The consequent parameters are updated using the Least Squares Estimation (LSE) method by calculating the error between the system output y and the target output y_t , based on the total dataset m. The error is defined as follows,

$$E = \frac{1}{2} \sum_{i=1}^{m} (y_i - y_{t,i})^2 \tag{7}$$

After that, in the second process, the backward pass is performed using the backpropagation method to minimize the error by updating the parameters c and σ of the membership function based on the calculated error. To update the parameter c, the following equation is used,

$$c_{new} = c_{old} - \eta \frac{\partial E}{\partial c} \tag{8}$$

where, $\frac{\partial E}{\partial c}$ is the partial derivative of the error concerning *c* and η is the learning rate. Then, to update the parameter σ , the following equation is used,

$$\sigma_{new} = \sigma_{old} - \eta \frac{\partial E}{\partial \sigma} \tag{9}$$

where, $\frac{\partial E}{\partial \sigma}$ is the partial derivative of the error concerning σ . This process is repeated until the error reaches a minimum value or until a certain number of iterations is reached.



FIGURE 3. Proposed triple-axis sun tracker

C. SUN TRACKER SYSTEM

Figure 3 shows the physical device of the sun tracker system. The proposed design implements a triple-axis mechanism with three manipulator arms. This mechanism allows the system to follow the sun's position more quickly as the motors move in parallel. The system uses servo motors as its actuators.



FIGURE 4. The movement of sun's position



In the testing process, the sun tracker system is compared with the sun's movement path to evaluate the performance of the proposed system. Figure 4 illustrates the position of the sun relative to the tracker. Two main parameters are used to determine the sun's position: azimuth and altitude. Azimuth is the horizontal angle measured clockwise from the north. An angle of 90° means the sun is in the east, 180° in the south, and 270° in the west. Azimuth indicates the sun's direction along the horizon [60]. Meanwhile, altitude measures the sun's height above the horizon, calculated from the horizontal line to the sun's position. This angle changes throughout the day, starting at 0° when the sun rises, reaching its peak at noon, and then returning to 0° when the sun sets [61]. The sun's movement path can be calculated using astronomical formulas based on location and time. The equation to calculate the solar azimuth angle (ϕ_s) is expressed as follows,

$$\sin\phi_S = \frac{\cos\delta \cdot \sin\gamma_H}{\cos\varphi_S} \tag{10}$$

where, δ is the solar declination angle, which can be calculated using the following equation,

$$\delta = 23.45^{\circ} . \sin\left(360 . \frac{284 + n}{365}\right) \tag{11}$$

where, *n* is the day number in the year. Meanwhile, γ_H is the solar hour angle, expressed as follows,

$$\gamma_H = 15^{\circ} \left(T_r - 12 \right) \tag{12}$$

where, T_r is the true time, ranging from 0 to 24 hours. Then, φ_s is the solar altitude angle, expressed as follows,

$$\sin \varphi_S = \sin \omega \, . \, \sin \delta + \cos \omega \, . \, \cos \delta \, . \, \cos \gamma_H \tag{13}$$

where, ω represents the latitude coordinate based on the location on earth.

III. PROPOSED METHOD

The proposed method includes ANFIS modelling and determining the most optimal consequent rule to be applied. It also explains the proposed mechanical structure in the sun tracker system, which aims to optimize the movement of the solar panels to enhance solar energy absorption efficiency. The modeling process of ANFIS and the simulation of the sun tracker system were conducted on a computer with an AMD Ryzen 5 4600H CPU, 16 GB DDR4 RAM, and an NVIDIA GeForce GTX 1650 Ti GPU with 4 GB memory. Additionally, the software used includes Python 3.10 with TensorFlow version 2.12.0. The flowchart illustrating the entire proposed system, including the ANFIS modeling method and sun tracker control, is shown in Figure 5.

A. ANFIS MODEL

In this study, ANFIS is used to control the movement of servo motors based on the light intensity readings from the

tetrahedron sensor. The rotation of the motors affects the movement of the manipulator arms, which direct the PV towards the sun. This study proposes ANFIS-PCT, consisting of three ANFIS models, each responsible for controlling a different motor, as shown in Figure 6, with the structure of each network shown in Table 3. The proposed membership function utilizes a Gaussian function chosen for its flexibility in modeling nonlinear relationships between inputs and outputs [62]. The number of membership functions for each input was determined based on performance evaluation through simulation, where three membership functions per input demonstrated a balance between computational complexity and model accuracy. Using more than three membership functions increases accuracy but significantly adds to computation time, making it unsuitable for real-time sun tracker systems. The learning rate parameter was set to 0.01 after testing, which showed that this value provides stable convergence without compromising training speed. Additionally, the number of training iterations was set to 5000 epochs based on observations indicating that the model achieves minimum error performance within this range.

TABLE 3. Proposed ANFIS structure

Parameter	Value	Description
Number of input	3	Number of nodes in the input layer
Number of output	1	Number of nodes in the output layer
Number of fuzzy MF 1	3	Number of membership functions at input node 1
Number of fuzzy MF 2	3	Number of membership functions at input node 2
Number of fuzzy MF 3	3	Number of membership functions at input node 3
Membership function	Gaussian function	Membership function at input
Number of rules	27	Number of rules fuzzy
Number of datasets	1945	Number of data for training process
Learning rate	0.01	ANFIS learning rate parameter

Based on Figure 6, ANFIS 1 model controls the angle (θ) of servo motor 1 based on inputs from P_1 sensor, P_2 sensor, and the initial angle (θ_0) of servo motor 1. ANFIS 2 model controls the angle of servo motor 2 based on inputs from P_2 sensor, P_3 sensor, and the initial angle of servo motor 2. Meanwhile, ANFIS 3 model controls the angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 5 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 5 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor , P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor , P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor , P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor , P_1 sensor , and the initial angle of servo motor 3 based on input sensor P_1 sensor , and the initial angle of servo motor 3 based on input sensor P_1 sensor P_1 sensor P_2 sensor P_1 sensor P_2 sensor P_3 sensor P_3

There is a consequent rule in defuzzification, obtaining results based on fuzzy rules by describing the mathematical relationship between input and output [63]. The parameters in the consequent rule are optimized during the training process to ensure that the model can accurately predict the output based on the given data. This paper proposes three





FIGURE 5. Flowchart of ANFIS modeling and solar tracking control system

types of consequent rules: polynomial functions of firstorder, second-order, and third-order. These consequent rules are applied to Eq. (5). The first-order function is expressed as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + r \tag{14}$$

where, $f(x_i)$ represents the output of the consequent rule, p_i is the first-order parameter for input x_i , and r is the bias constant of the rule. Meanwhile, for the second-order function, the equation is as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + \sum_{i=1}^{3} q_i x_i^2 + \sum_{1 \le i < k \le 3} c_{i,k} x_i x_k + r \quad (15)$$

where, q_i is the second-order parameter for input x_i and $c_{i,k}$ is the parameter for the cross terms between inputs x_i and x_k . Then, for the third-order function, the equation is as follows,

$$f(x_i) = \sum_{\substack{i=1\\3}}^{3} p_i x_i + \sum_{\substack{i=1\\3}}^{3} q_i x_i^2 + \sum_{\substack{1 \le i < k \le 3\\1 \le i < k \le 3}} c_{i,k} x_i x_k + \sum_{\substack{i=1\\i=1}}^{3} t_i x_i^3 + r$$
(16)

where, t_i is the second-order parameter for input x_i .

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B. MECHANICAL STRUCTURE OF SUN TRACKER

This sun tracker system configuration uses three manipulator arms, as shown in Figure 7. The model of the manipulator arms is arranged in a parallel configuration, with servo motors as the actuators. These three arms are connected to a triangular plane that serves as the base for the PV. Points J_1 , J_2 , and J_3 connect the plane to the manipulator arms. The height of these points will affect the orientation of the PV in following the sun's movement.



FIGURE 7. Triple-arm manipulator configuration on sun tracker system



FIGURE 8. The configuration of arm manipulator: (a) arm structure design, (b) system mechanism

The configuration of the manipulator arm is shown in Figure 8(a). The arm consists of the upper arm (b_i) and the lower arm (a_i) , with lengths of 3.7 cm and 1.6 cm, respectively. Additionally, there are two connection points: the elbow point (E_i) and the end-effector point (J_i) , as well as a drive point M_i as the motor (for i = 1,2,3). The E_i point is the connection between the lower and upper arm, while J_i is the connection between the upper arm and the base plane where the PV is mounted. Figure 8(b) shows the drive mechanism of the manipulator arm. The angle β_i is the orientation angle of the manipulator arm relative to the *x*-axis. The movement of motor M_i will create an angle θ_i . This angle



will affect the value of angle α_i at point E_i , causing the coordinates at point J_i to change. These coordinate changes can be calculated using the following forward kinematic equation [64], [65],

$$J_i x = (a_i \cos \theta_i + b_i \cos(\theta_i + \alpha_i)) \cos \beta_i + M_i x \quad (17)$$

$$J_i y = (a_i \cdot \cos \theta_i + b_i \cdot \cos(\theta_i + \alpha_i)) \sin \beta_i + M_i y \quad (18)$$

$$J_i z = a_i . \sin \theta_i + b_i . \sin(\theta_i + \alpha_i) + M_i z$$
(19)

By applying trigonometric theorems, we obtain,

$$J_i x = (a_i \cdot \cos \theta_i + b_i (\cos \theta_i \cdot \cos \alpha_i - \sin \theta_i \cdot \sin \alpha_i)) \cos \beta_i + M_i x$$
(20)

$$J_i y = (a_i \cdot \cos \theta_i + b_i (\cos \theta_i \cdot \cos \alpha_i - \sin \theta_i \cdot \sin \alpha_i))$$

$$\sin \beta_i + M_i y$$
(21)

$$J_i z = (a_i \cdot \sin \theta_i + b_i (\sin \theta_i \cdot \cos \alpha_i + \cos \theta_i \cdot \sin \alpha_i)) + M_i z$$
(22)

In this condition, the arm b_i remains perpendicular at 90° to the base, even when motor M_i moves. This is because point J_i is connected to the triangular plane above it, keeping arm b_i perpendicular. The simulation of this movement is shown in Figure 9. Based on this condition, the angle $\alpha_i = 90 + \theta_i$, so by applying the rules $cos(90 + \theta_1) = -sin \theta_i$ and $sin(90 + \theta_1) = cos \theta_i$, we obtain $sin \alpha_i = cos \theta_i$ and $cos \alpha_i = -sin \theta_i$. Then, by substituting in Eq. (20), Eq. (21), and Eq. (22), the following equations is derived.

For the point x,

$$J_{i}x = (a_{i} \cos \theta_{i} + b_{i}(-\cos \theta_{i} \sin \theta_{i} - \sin \theta_{i} \cos \theta_{i}) \cos \beta_{i} + M_{i}x$$
(23)

$$J_i x = (a_i \cdot \cos \theta_i + b_i (-2 \sin \theta_i \cdot \cos \theta_i) \cos \beta_i + M_i x \quad (24)$$

$$J_i x = (a_i \cdot \cos \theta_i + b_i \cdot \sin 2\theta_i) \cdot \cos \beta_i + M_i x$$
⁽²⁵⁾

For the point *y*,

$$J_{i}y = (a_{i} \cos \theta_{i} + b_{i}(-\cos \theta_{i} \sin \theta_{i} - \sin \theta_{i} \cos \theta_{i}) \\ \sin \beta_{i} + M_{i}y$$
(26)

$$J_i y = (a_i \cdot \cos \theta_i + b_i (-2 \sin \theta_i \cdot \cos \theta_i) \sin \beta_i + M_i y \quad (27)$$

$$J_i y = (a_i . \cos \theta_i + b_i . \sin 2\theta_i) . \sin \beta_i + M_i y$$
(28)

For the point z,

$$J_{i}z = (a_{i}.\sin\theta_{i} + b_{i}(-\sin\theta_{i}.\sin\theta_{i} + \cos\theta_{i}.\cos\theta_{i}) + M_{i}z$$
(29)

$$J_i z = (a_i \sin \theta_i + b_i (1 - 2\sin^2 \theta_i) + M_i z$$
(30)

$$J_i z = a_i \sin \theta_i + b_i \cos 2\theta_i + M_i z \tag{31}$$

In the proposed system, the angle β_i varies for each motor. In Figure 10(a), the top view shows the orientation of motors M_1 , M_2 , and M_3 , each connected to arms a_1 , a_2 , and a_3 at points E_1 , E_2 , and E_3 . The angle between each motor is depicted, with 315° for M_1 , 45° for M_2 , and 180° for M_3 . Meanwhile, Figure 10(b) shows the physical layout or placement positions of the motors and the manipulator arms connected at the same points. These motors are strategically positioned to move each arm accurately.



FIGURE 9. Principle work of manipulator arm movement: (a) downward movement, (b) upward movement



FIGURE 10. The arrangement of servo motors from a top view: (a) orientation of each motor, (b) position of each motor



FIGURE 11. The normal vector on the triangular plane



Next, the tracker system's azimuth and altitude direction are calculated based on each motor's movement angle. To determine these values, it is necessary to calculate the normal vector of the triangular plane, as shown in Figure 11, where $\overrightarrow{v_0}$ is the initial normal vector when its direction is perpendicular upward, and \overrightarrow{v} is the normal vector when its direction changes. Based on the coordinate points $J_1(x_1, y_1, z_1), J_2(x_2, y_2, z_2)$, and $J_3(x_3, y_3, z_3)$, the normal vector is calculated using the following equation,

$$\vec{\nu} = \vec{J_1 J_2} \cdot \vec{J_1 J_3} \tag{32}$$

where, $\overline{J_1J_2}$ is the vector from point J_1 to point J_2 and $\overline{J_1J_3}$ is the vector from point J_1 to point J_3 . The vectors in Eq. (32) can be calculated using the following equations,

$$\overrightarrow{J_1J_2} = (x_2 - x_1, y_2 - y_1, z_2 - z_1)$$
(33)

$$\overrightarrow{J_1J_3} = (x_3 - x_1, y_3 - y_1, z_3 - z_1)$$
(34)

Thus, from Eq. (33) and Eq. (34), the normal vector is expressed as follows,

$$\vec{v} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ x_2 - x_1 & y_2 - y_1 & z_2 - z_1 \\ x_3 - x_1 & y_3 - y_1 & z_3 - z_1 \end{vmatrix}$$
(35)

So that, we obtain,

$$v_{x} = (y_{2} - y_{1})(z_{3} - z_{1}) - (y_{3} - y_{1})(z_{2} - z_{1})$$
(36)

$$v_y = (x_2 - x_1)(z_3 - z_1) - (x_3 - x_1)(z_2 - z_1)$$
(37)

$$v_z = (x_2 - x_1)(y_3 - y_1) - (x_3 - x_1)(y_2 - y_1)$$
(38)

Based on Eq. (36), Eq. (37), and Eq. (38), the tilt angle of the plane concerning the *x*-axis (θ_x) and the *y*-axis (θ_x) can be determined using the following equations,

$$\theta_x = \cos^{-1}\left(\frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}}\right)$$
(39)

$$\theta_{y} = \cos^{-1} \left(\frac{v_{y}}{\sqrt{v_{x}^{2} + v_{y}^{2} + v_{z}^{2}}} \right)$$
(40)

Meanwhile, to calculate the tracker azimuth (ϕ_T) and tracker altitude (φ_T), the following equations are used,

$$\phi_T = tan^{-1} \left(\frac{v_y}{v_x} \right) \tag{41}$$

$$\varphi_T = tan^{-1} \left(\frac{v_z}{\sqrt{v_x^2 + v_y^2}} \right) \tag{42}$$

Meanwhile, point G is the centroid of the triangle and can be calculated using the following equation,

$$\begin{bmatrix} G_x \\ G_y \\ G_z \end{bmatrix} = \begin{bmatrix} (x_1 + x_2 + x_3)/3 \\ (y_1 + y_2 + y_3)/3 \\ (z_1 + z_2 + z_3)/3 \end{bmatrix}$$
(43)

IV. PERFORMANCE ANALYSIS

The analysis provides performance results of each model in predicting PV output power based on its operational temperature. The analytical methods used include calculating Mean Absolute Error (MAE), Root Mean Squared Error (RMSE), Mean Absolute Percentage Error (MAPE), Coefficient of Determination (R^2), and Coefficient of Variation (CV).

MAE is one of the commonly used methods to analyze model performance. It measures the average absolute difference between the predicted values generated by the model and the actual values in the test data. This result shows how closely the model predictions match the actual values overall. The equation for MAE is as follows,

$$MAE = \frac{1}{n} \sum_{i=n}^{n} |y_i - \hat{y}_i|$$
(44)

where, *n* is the number of test data points, y_i is the actual value, and \hat{y}_i is the value predicted by the model for the *i* data point. A lower MAE value indicates better model performance, signifying that the model's predictions are closer to the actual values [66]. Next, RMSE analysis is conducted by calculating the square root of the average of the squared differences between the model's predicted values and the actual values. The equation for RMSE is defined as follows,

$$RMSE = \sqrt{\frac{1}{n} \sum_{i=n}^{n} (y_i - \hat{y}_i)^2}$$
(45)

RMSE analysis indicates the average deviation between the model's predicted and actual values. By taking the square root, RMSE offers a more intuitive interpretation in the same units as the target variable. A lower RMSE value indicates better model performance, meaning the model's predictions are closer to the actual values [67]. Next, MAPE analysis is a method to measure the error rate of a model by calculating the average of the absolute percentage error between the predicted and actual values. The equation for calculating MAPE is defined as follows,

$$MAPE = \frac{1}{n} \sum_{i=n}^{n} \left| \frac{y_i - \hat{y}_i}{y_i} \right| .100\%$$
(46)

The MAPE value indicates the prediction error in percentage terms. The lower the MAPE value, the better the model's performance in predicting the data. One advantage of MAPE is its ease of interpretation, as the result is a percentage. Next, the R^2 analysis, known as the Coefficient of Determination, is used to measure how well the developed model can explain the variability in the data. The equation for the Coefficient of Determination is defined as follows,

$$R^{2} = 1 - \frac{\sum_{i=1}^{n} (y_{i} - \hat{y}_{i})^{2}}{\sum_{i=1}^{n} (y_{i} - \hat{y})^{2}}$$
(47)

where, \hat{y} is the mean of all y_i values. The R^2 value ranges from 0 to 1, where a value closer to 1 indicates that the model better explains the variability in the data. R^2 analysis can determine how much output data variability can be explained by the input data. Lastly, the CV analysis, or Coefficient of Variation, is a statistical measure to assess a dataset's relative degree of variation. CV is defined as the ratio of the standard deviation to the mean, expressed as follows,

$$CoV = \frac{\sqrt{\frac{1}{n}\sum_{i=1}^{n} \left(y_{i} - \frac{1}{n}\sum_{i=1}^{n} y_{i}\right)^{2}}}{\frac{1}{n}\sum_{i=1}^{n} y_{i}}$$
(48)

CV is typically used to measure data stability. A low CV value indicates more stable data, while a high CV value suggests more significant variability in the data.

V. RESULTS AND DISCUSSION

In this section, an evaluation is conducted to assess the performance of ANFIS in each model based on the type of consequent rule. Then, the movement of the three motors is simulated to obtain the azimuth and altitude angles. Testing uses the sun tracker device to assess the system's ability to track the sun's position. Finally, comparing previous systems is necessary to validate the proposed sun tracker system's effectiveness.

A. MODEL PERFORMANCE ANALYSIS

Table 4 presents the statistical results from the model's training and testing phases based on three types of consequent rules: first-order, second-order, and third-order. The dataset consists of 80% for training and 20% for testing. The ANFIS training and testing results show that the choice of consequent rule significantly impacts each model's performance.







FIGURE 12. The comparison analysis of consequence rule variations to controlling motor movements (a) ANFIS 1 model, (b) ANFIS 2 model, (c) ANFIS 3 model

In ANFIS model 1, the second-order performed best compared to the first-order and third-order, both in the training and testing phases. During training, the second-order achieved the lowest MAE, RMSE, and MAPE values, at 3.6, 4.5, and 8.08%, respectively, along with a high R^2 value of 0.98. This result indicates that the model can predict motor movement accurately based on the input data. In testing, the second-order also excelled with the lowest MAE, RMSE, and MAPE values, at 2.82, 3.34, and 7.02%, respectively, indicating accurate model performance with minimal error. In ANFIS model 2, a similar pattern emerged, with the secondorder demonstrating optimal performance. During training, the second-order model yielded low MAE, RMSE, and MAPE values of 3.82, 4.74, and 8.3%, along with a high R^2 value of 0.97. In testing, the second-order produced MAE, RMSE, and MAPE values of 3, 3.58, and 6.44%, respectively, outperforming the first-order and third-order models. In ANFIS model 3, the second-order also provided the best results, achieving the lowest error values in training with MAE, RMSE, and MAPE of 3.8, 4.68, and 7.69%, respectively, and the highest R^2 value of 0.98. However, in testing, the second-order's performance was less optimal than the third-order, as indicated by higher MAE, RMSE, and MAPE values than the third-order. The training and testing



analysis results show that the second-order consequent rule is optimal for all three ANFIS models.



FIGURE 13. The relationship between the phototransistor ratio values with the motor angle increases based on various consequent rules: (a) first-order, (b) second-order, and (c) third-order

Figure 12(a) displays the motor movement results with different consequent rules. The graph shows that all three consequent rules follow the angle change patterns quite well, although first-order shows more significant discrepancies. Meanwhile, in Figure 12(b), the first-order consequent rule exhibits noticeable differences, especially in the sixth and eighth experiments. On the other hand, second-order and third-order are more consistent in approaching the actual

angle, although slight differences still exist at some points. In Figure 12(c), the average difference between the actual angle and the angle produced by each consequent rule is more minor than the previous graph. Overall, although both second-order and third-order consequent rules accurately follow the angle change patterns of all three motors, there are some points where the second-order performs better than the third-order. Figure 13 shows a three-dimensional graph illustrating the relationship between the ratio of two phototransistor values and the output as the motor angle increments for each consequent rule. The comparison values from the two phototransistor readings directly affect the magnitude of the resulting angle increment. In the first-order consequent, the angle increment pattern appears linear. In the second-order consequent, a significant angle increment occurs with more considerable phototransistor ratio differences; the greater the difference, the higher the angle increment. Conversely, there is no considerable angle increase for ratios closer in value. In the third-order, the angle increment pattern is similar to the second-order but displays fluctuations or a nonlinear pattern in the middle of the graph. This indicates that there are points where small changes in the phototransistor ratio can lead to a lower or even decreasing angle increment.



FIGURE 14. The simulation of azimuth and altitude changes based on motor movement ($M_1 = 26^\circ, M_2 = 40^\circ, M_3 = -30^\circ$)

After obtaining the model, a motor movement simulation was conducted on the sun tracker to observe the relationship between the movements of the three motors and changes in azimuth and altitude angles. Figure 14 displays the simulation results, showing how each motor's activity influences the panel's orientation changes. In this simulation, it demonstrates the condition where the three motors move at angles $M_1 = 26^\circ$, $M_1 = 40^\circ$, and $M_1 = -30^\circ$, resulting in a normal vector direction of (0, 8, 26) with tilt angles of $\theta_x =$ 90° and $\theta_y = 72^\circ$. Meanwhile, the resulting azimuth and altitude angles are 89° and 72°, respectively. Further testing



Madal	Demonster	Training			Testing			
Model	Parameter	First-Order	Second-Order	Third-Order	First-Order	Second-Order	Third-Order	
	MAE	9.3	3.6	5.26	9.57	2.82	4.08	
	RMSE	11.61	4.5	6.21	11.33	3.34	4.95	
ANFIS 1	MAPE	21.79%	8.08%	17.08%	21.78%	7.02%	10.5%	
	\mathbb{R}^2	0.81	0.98	0.96	0.83	0.99	0.97	
	CV	0.39	0.49	0.47	0.42	0.47	0.44	
	MAE	11.09	3.82	5.08	9.79	3	3.51	
	RMSE	13.78	4.74	6.05	11.81	3.58	4.33	
ANFIS 2	MAPE	19.44%	8.3%	12.86%	21.57%	6.44%	8.79%	
	\mathbb{R}^2	0.69	0.97	0.95	0.82	0.99	0.98	
	CV	0.3	0.42	0.4	0.4	0.46	0.46	
	MAE	11.76	3.8	4.41	8.94	2.86	2.77	
	RMSE	14.1	4.68	5.33	10.86	3.48	3.4	
ANFIS 3	MAPE	22.83%	7.69%	8.83%	18.52%	6.35%	6.11%	
	R ²	0.7	0.98	0.97	0.85	0.99	0.99	
	CV	0.35	0.48	0.43	0.41	0.47	0.47	

TABLE 4. The results of ANFIS training and testing with various consequent rules



FIGURE 15. The results of the sun tracker movement experiment based on all combinations of angles M_1 , M_2 , and M_3 : (a) azimuth angle movement and (b) altitude angle movement

results are shown in Figure 15, combining an angle range of -30° to 90°, representing the minimum to maximum motor angles. Figure 15(a) shows that the azimuth angle ranges from 0° to 360°, while Figure 15(b) indicates that the altitude angle ranges from 60° to 90°. This angle range demonstrates that the

triple-axis mechanism can achieve good orientation flexibility, allowing the system to adjust the PV panel position effectively to minimize the solar incidence angle.

Subsequent testing was conducted to analyze the response of the sun tracker system in mitigating uncertain disturbances, such as the continuous movement of light due to cloud movement or shadows from external objects. The testing scenario involved observing the movement of the sun tracker at azimuth and altitude angles of 89° and 72°, respectively. The results of the sun tracker system's response based on ANFIS consequent rules are shown in Figure 16. Based on these tests, the proposed control rules were able to mitigate the effects of disturbances, such as changes in light intensity due to clouds, while maintaining the optimal orientation of the solar panel. Under partial shading conditions, where some sensors or PV panels receive reduced light intensity due to shadows from clouds or surrounding objects, the tracking system may face challenges in maintaining the optimal orientation of the solar panel toward the sun.





FIGURE 16. The comparison result of responses to light changes for each ANFIS consequent rules (a) azimuth movement, (b) altitude movement

Further analysis was conducted to determine the system's response to each ANFIS consequent rule in response to changes in light position. The study was performed by comparing the system's response based on Figure 16. This analysis considered characteristics such as rise time, peak time, overshoot, settling time, and steady-state error for both azimuth and altitude movements, which are presented in Table 5 and Table 6. For azimuth movement, second-order showed the most optimal performance, achieving the fastest rise time and settling time with low steady-state error. The second-order response also did not exhibit any overshoot. Meanwhile, the peak time obtained was longer than that of the first-order. In the first-order, the settling time was unavailable because the system response did not reach a steady-state condition during the observation period. For altitude movement, the analysis also indicated that the second-order performed better than the others. No overshoot occurred in the second-order, as with the azimuth movement. In the first-order, the settling time was also unavailable, as the system response did not reach a steady-state condition. This analysis reveals that second-order is the best choice for controlling both azimuth and altitude movements, making this consequent rule most suitable for implementation in ANFIS-PCT for a triple-axis sun tracker system.

 TABLE 5.
 The comparison of performance ANFIS consequent rules on azimuth movement

Parameter	First-order	Second-order	Third-order
Rise Time (s)	0.681	0.601	0.661
Peak Time (s)	1.403	1.723	1.483
Overshoot (%)	0.899	0	0.562
Settling Time	-	1.462	2.212
Steady State Error	0.679	0.03	0.111

 TABLE 6. The comparison of performance ANFIS consequent rules on altitude movement

Parameter	First-order	Second-order	Third-order
Rise Time (s)	0.511	0.491	0.521
Peak Time (s)	2.685	1.493	1.283
Overshoot (%)	0.556	0	0.139
Settling Time	-	1.34	1.538
Steady State Error	0.399	0.027	0.213



B. SUN TRACKER SYSTEM PERFORMANCE ANALYSIS Figure 17(a) compares the sun tracker movement and the azimuth angle of the actual sun position. The graph shows the sun tracker accurately follows the sun's azimuth angle from sunrise to sunset. Meanwhile, Figure 17(b) compares the altitude angle. Based on this graph, a discrepancy occurs at the start of tracking, around 7:00 AM to 8:00 AM. Then, the sun tracker successfully tracks the sun's altitude more accurately, reaching a peak at 12:30 PM at its maximum altitude. Afterwards, the altitude of the sun tracker gradually decreases in sync with the sun's position until sunset. Overall, the sun tracker system works effectively to adjust its movement in tracking the sun's position in azimuth and altitude angles, thereby minimizing the solar incidence angle on the PV surface throughout the day.



FIGURE 17. The result comparison between the tracked and the sun's actual position: (a) azimuth movement and (b) altitude movement

C. SYSTEM PERFORMANCE COMPARISON

Table 7 compares the proposed ANFIS model's performance with several previous models related to sun tracker systems. The comparison aims to validate the performance of the proposed ANFIS model in tracking the sun's position. The models compared include PID-ANN [44], Fast Integral Terminal Sliding Mode Control (FIT-SMC) [68], Neural Network Algorithm with Model Predictive Control (NNA-MPC) [69], PID with Internal Model Controller (PID-IMC) [51], PID with Fuzzy Logic Controller (PID-FLC) [48], PD with Fuzzy Logic Controller (PD-FLC) [46], and Artificial Bee Colony (ABC) [50]. The parameters compared are rise time, settling time, and steady-state error. Based on the comparison, the proposed ANFIS-PCT model demonstrates optimal performance. For the rise time parameter, ANFIS-PCT has a relatively fast time, only behind the FIT-SMC model, which recorded the most rapid rise time of 0.15 seconds. However, compared to other models,



ANFIS-PCT is far superior. For the settling time parameter, ANFIS-PCT also shows optimal performance, although it is still behind FIT-SMC, which recorded the fastest time. Meanwhile, for the steady-state error, ANFIS-PCT demonstrates a more stable and accurate system.

 TABLE 7. The comparison of the proposed ANFIS model with other published models

Rise Time (s)	Settling Time (s)	Steady State Error
0.55	1.4	0.03
2.18	2.46	0.07
0.15	0.33	-
-	0.108	-
1.8	5.58	-
3.6	4.8	0.4
6.38	6.38	0.83
2.37	5.23	1.05
	Rise Time (s) 0.55 2.18 0.15 - 1.8 3.6 6.38 2.37	Rise Time (s) Settling Time (s) 0.55 1.4 2.18 2.46 0.15 0.33 - 0.108 1.8 5.58 3.6 4.8 6.38 6.38 2.37 5.23

VI. CONCLUSION

Based on the analysis results, all three proposed ANFIS models using the second-order consequent rule deliver the best performance compared to the first-order and third-order, both in the training and testing phases. The simulation results show that the movement of the sun tracker with a triple-axis mechanism can reach an azimuth angle ranging from 0° to 360°. In contrast, the altitude angle ranges from 60° to 90°. These values indicate that the sun tracker has good flexibility. The proposed system has nonlinear dynamics, so several parameters must be continuously optimized through the training process to gradually reduce the error value in the system until it approaches zero. This indicates that the system will always move towards stability, even with small variations in input parameters or disturbances.

Although the proposed sun tracker system offers improved accuracy and responsiveness in tracking the sun's position, it has some drawbacks, including system complexity, leading to higher energy consumption. This is due to the number of motors that need to move simultaneously to reach the optimal position. The additional energy the motors consume in the triple-axis mechanism can reduce overall energy efficiency, especially in conditions with limited energy sources.

Future research will focus on developing triple-axis sun tracker technology techniques to enhance efficiency by reducing energy consumption and optimizing PCT in ANFIS to make it more adaptive in tracking the sun's position. Further research can be developed by exploring the Lyapunov method to explicitly determine the stability of the sun tracker system, allowing the mathematical proof to support the experimental results that have been conducted. Additionally, future research will focus on exploring energy-saving strategies, including optimizing by reducing unnecessary servo motor movements, as well as evaluating the comparison between the energy produced and the total energy consumed.

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ANFIS Parallelization Control on Triple-Axis Sun Tracker to Minimize Solar Rays Incidence Angle on Photovoltaic

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ABSTRACT This study proposes an Adaptive Neuro-Fuzzy Inference System (ANFIS) based on model with Parallelization Control Technique (PCT) implemented in a triple-axis sun tracker system. The system aims to maximize solar energy absorption by minimizing the angle of incidence of sunlight on Photovoltaic (PV) panels. It is designed with three manipulator arms, each controlled in parallel by a distinct ANFIS model. The primary goal is to adjust the PV panel orientation to optimal azimuth and altitude angles. A tetrahedron sensor is employed to detect the direction of sunlight. This study tests various types of consequent rules to find the optimal configuration for each ANFIS model, including first-order, second-order, and third-order polynomial functions. The analysis results show that the second-order consequent rule provides the highest accuracy across the three ANFIS models. The proposed system can cover an azimuth range from 0° to 360° and an altitude angle from 60° to 90°. The experiment also demonstrated that the system consistently moves toward a stable condition, even in the presence of minor disturbances. These findings indicate that ANFIS with PCT can minimize the angle of sunlight incidence, enhance system flexibility, and accelerate response time, making it a viable solution for increasing energy harvesting by PV panels.

INDEX TERMS ANFIS, parallelization control, photovoltaic, sun tracker, triple-axis

I. INTRODUCTION

The sun tracker system is designed to automatically follow the sun's movement, maximizing sunlight reception on Photovoltaic (PV) panels [1]. This technology is essential in increasing energy production in PV systems, especially in areas with high sunlight intensity. PV efficiency heavily depends on the angle of sunlight incidence on the PV surface. The more optimal the angle, the greater the amount of sunlight absorbed, increasing the electrical energy produced [2], [3]. To maximize generated energy, the orientation of the panels needs to be adjusted in real-time so that the PV always maintains an optimal angle to the sunlight [4]–[6]. Conventional solar power plants are generally installed statically, so PV panels do not receive optimal sunlight exposure, especially in the morning and evening [7], [8]. A sun tracker system can dynamically

[9]–[11]. Sun tracker systems have been discussed in several studies, including in [12], where a comparison between fixed PV systems and sun trackers was conducted. The results showed that sun trackers can increase electricity generation by 30% compared to fixed PV systems. Another study in [13] examined a sun tracker system using a Stewart platform mechanism, demonstrating that the sun tracker system can enhance energy generation by 32% compared to fixed PV systems. Additionally, [14] compares energy produced and consumed by sun tracker systems. The findings indicate that the total energy obtained from a sun tracker system is 26.9% higher than from a fixed PV system, with the energy consumption of the sun tracker reaching 5.63% or around 21.22 Wh and total energy production of

adjusted the PV orientation to remain perpendicular to the

sunlight, thereby maximizing the electrical energy obtained



376.85 Wh. These studies show that sun trackers are superior to fixed PV systems. Furthermore, as discussed in [15], the popularity of sun tracker systems continues to rise along with the growing use of solar energy as an alternative energy source. Further developments in sun tracker systems cover various aspects, including manual control through internet networks as studied in [16], [17], bluetooth-based control as examined in [18], and automatic control using solar trajectory models as explored in [19], [20].

In its implementation, a sun tracker requires an effective sensor to accurately detect the sun's position coordinates. This study proposes a type of sensor called a tetrahedron sensor. The survey of the tetrahedron sensor was first introduced in [21], which analyzed the design and structure of the sensor, consisting of three photoresistors. The study's results demonstrated that the tetrahedron sensor could detect the sun's position with a maximum wide Field of View (FOV) of 289.4° and an accuracy of $\pm 1.67^{\circ}$. Further research on the tetrahedron sensor is discussed in [22], which focuses on developing a sensor based on phototransistors to replace photoresistors. Additionally, [23] examined the effect of the tetrahedron sensor's dimensions on the sun tracker's performance in tracking the sun's position. The results showed that increasing the height of the tetrahedron correlates with an increase in FOV, where a tetrahedron with a height of 4.5 cm has an FOV of 289.4°, while a height of 10.2 cm reaches an FOV of 310°.

An appropriate control algorithm and drive mechanism are needed to control the orientation movement of a sun tracker. The control algorithm is necessary to quickly and stably adjust the panel position, reducing energy losses caused by suboptimal angles of incidence. Meanwhile, the drive mechanism is required to support smooth and precise movements. Several studies have examined single-axis and dual-axis drive mechanisms with various algorithms, as shown in Table 1. Based on these studies, the design of the control mechanism in a sun tracker significantly influences the system's response time in following the sun's movement. On the other hand, some studies have developed triple-axis drive mechanisms. This mechanism is designed to improve the vertical orientation adjustment of PV panels. In [24], it is stated that the efficiency of commercial PV typically ranges from 10-20%. Applying a triple-axis mechanism to the sun tracker increases PV efficiency by up to 25%. In [25], it is revealed that the power output generated by PV on a triple-axis sun tracker is 19% greater than that of a dual-axis mechanism. This improvement is due to the triple-axis mechanism's ability to adjust the PV panel's height, enabling it to prevent shadows from surrounding objects from falling onto the panel surface. Furthermore, [26] states that a triple-axis sun tracker can be implemented on a mobile platform, allowing the panel to adjust its orientation to maintain an optimal position even if the platform moves. Although triple-axis sun trackers have significant potential for improving PV efficiency, there are still technical challenges in determining a control method to

optimize panel orientation. With the proper control method, the system can adapt to changes in the sun's position and avoid shadows from objects falling on the panel surface [27]. One approach capable of adapting to changing conditions is the Adaptive Neuro-Fuzzy Inference System (ANFIS).

ANFIS is an algorithm that combines approaches from Artificial Neural Networks (ANN) and Fuzzy Inference Systems (FIS) to model complex relationships between inputs and outputs [28]. FIS handles uncertain data using fuzzy rules and membership functions to map input values into fuzzy sets [29]. Meanwhile, ANN is responsible for the learning process, where parameters within the fuzzy system, such as membership functions and fuzzy rules, are automatically optimized based on the provided training data [30]. The main processes in ANFIS include fuzzification, which transforms input values into fuzzy values; fuzzy inference, which generates fuzzy output based on fuzzy rules; and defuzzification, which converts the fuzzy output into a numerical value [31], [32]. Several studies have explored the application of ANFIS in various fields. For example, in [33], ANFIS was applied to model machine behaviour in a gas turbine by estimating its operational parameters and improving its performance and durability. Furthermore, [34] discusses the application of ANFIS for controlling dynamic force and position in a Programmable Universal Machine for Assembly (PUMA) robot. Another study [35], applied ANFIS to model the behaviour of an air spring system, which was used to control the solenoid valve of the air spring system to reduce mass acceleration. In addition, other studies have discussed the application of ANFIS in controlling sun trackers. For instance, [36] compared the performance of a Proportional Integral Derivative (PID) controller with ANFIS, with both algorithms optimized using the Firefly Algorithm (FA) to enhance system speed and stability. The findings showed that the ANFIS-FA combination significantly reduced overshoot and accelerated settling time. Furthermore, [37] explored the ANFIS application by comparing single-axis and dual-axis sun tracker mechanisms, concluding that ANFIS with five membership functions was more optimal in controlling both sun tracker mechanisms, yielding high prediction accuracy and low error. Additionally, [38] conducted further analysis on ANFIS as a sun tracker controller, examining the effect of the number of membership functions on model training. This study revealed that the number of membership functions directly affects model performance, with an increase in membership functions leading to reduced error. Moreover, ANFIS offers the flexibility of fuzzy logic, enabling it to learn from data automatically adjust parameters and [39]. The implementation of ANFIS is less complex compared to other control methods, such as Linear Quadratic Regression (LQR) and Model Predictive Control (MPC). MPC has significantly higher complexity than ANFIS, as it requires solving optimization problems at each time step to



Paper	Year	Algorithm	Control Mechanism	Rise Time (s)	%Error
Yuwaldi Away et al. [44]	2023	PID-ANN	Dual-Axis	2.18	1.75%
Andri Novandri et al. [45]	2022	PID	Dual-Axis	1.85	2.6%
Fitri Rahmah et al. [46]	2022	Fuzzy-PD	Single-Axis	7.43	0.43%
Baisrum et al. [47]	2021	ANFIS	Single-Axis	-	1.25%
Imam Abadi et al. [48]	2020	Fuzzy-PID	Dual-Axis	8.2	-
Jalal Farazi et al. [49]	2020	PO-ANN	Dual-Axis	0.94	-
Zubairu A. Yusuf et al. [50]	2019	ABC	Single-Axis	2.37	-
Bamigboye O. Oladayo et al. [51]	2016	IMC-PID	Dual-Axis	1.78	-
Mirza Muhammad Sabir et al. [52]	2016	PID	Dual-Axis	2.2	0.5%

TABLE 1. Literature review of control mechanism on sun tracker

determine the optimal control signal [40]. Additionally, LQR has low complexity because it only requires solving a functional quadratic equation. However, LQR is not designed to handle nonlinear systems, such as a triple-axis sun tracker [41]. Meanwhile, the ANFIS approach, which is a hybrid algorithm combining ANN and FIS, can quickly adjust parameters. This makes it highly suitable for realtime systems that demand quick responses and the ability to maintain responsiveness to environmental changes [42], [43]. Based on these studies, it is concluded that the ANFIS model can improve control performance in sun tracker systems, especially with additional optimization or increased membership functions. This makes ANFIS a practical approach for controlling PV panel orientation.

Based on these studies, most current sun tracker systems still rely on single-axis or dual-axis mechanisms, which have limitations in vertical adjustments and in avoiding shadows from objects surrounding the panels. On the other hand, research on triple-axis mechanisms is still minimal. Additionally, optimization techniques are needed to enhance the performance of the ANFIS algorithm in managing the complexity of sun tracker systems, particularly in triple-axis mechanisms. As a solution, the sun tracker system with a triple-axis drive mechanism is proposed. This proposed mechanism uses three manipulator arms, each driven by a servo motor. These three arms adjust the PV panel orientation along three axes, allowing the sun tracker to control movement at azimuth and altitude angles. A tetrahedron sensor consisting of three phototransistors arranged on each side of the tetrahedron, detects the sun's position. Additional optimization of the ANFIS algorithm is proposed to control the servo motors by applying the Parallelization Control Technique (PCT). This control method aims to divide computational processes into parts that can be executed in parallel, thereby enhancing computational efficiency and processing speed, especially in complex tasks. PCT enables multiple control processes to run simultaneously, reducing latency and improving system responsiveness. ANFIS-PCT offers an optimal balance between computational complexity, robustness against nonlinearity, and real-time responsiveness, making it the

best solution for triple-axis sun tracker systems. In this proposed sun tracker, the system is divided into three processes that are responsible for controlling each servo motor's rotation angle. Input data is obtained from the tetrahedron sensor readings, with input variables varying for each process, resulting in distinct ANFIS models. ANFIS modelling is conducted by designing the network structure, determining the membership functions, and establishing fuzzy rules. Within the fuzzy rules is a consequent rule, part of the fuzzy rule that defines the output based on the fulfilled input conditions. An analysis of the consequent rules is necessary to achieve an optimal model. This study examines three types of consequent rules to identify the most optimal model. The three types of proposed consequent rules are polynomial functions of first-order, second-order, and thirdorder. Each of these orders has different complexity and mapping capabilities in identifying the relationship between inputs and outputs, requiring evaluation to determine the most suitable model for the sun tracker. This research focuses on minimizing the solar incidence angle to enhance the electrical energy production of PV systems. When the solar incidence angle on the panel surface approaches zero, the amount of sunlight absorbed by the PV reaches its maximum, directly increasing the generated electrical output.

The novelty of this research lies in the implementation of PCT in ANFIS, which enables the division of computational processes into multiple parts running concurrently. Additionally, this study analyzes various consequent rule configurations in the ANFIS model, including first-order, second-order, and third-order polynomial functions, to determine the most optimal configuration. The main contributions of this paper are as follows:

- We propose a sun tracker system using a triple-axis mechanism consisting of three manipulator arms to control the azimuth and altitude angles. This system enables PV panels to adjust their angles optimally to the direction of incoming sunlight.
- We propose an ANFIS algorithm with PCT to control the movement of the sun tracker through separate

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control processes, making the system more responsive and accurate.

 We demonstrate that the second-order consequent rule provides the best performance in controlling the sun tracker, effectively minimizing the angle of incoming sunlight on the PV panel.

For convenience, the abbreviations used in this paper are summarized in Table 2.

TABLE 2. Summary of abbreviations

Abbreviation	Meaning
ANFIS	Adaptive Neuro-Fuzzy Inference System
ANN	Artificial Neural Networks
CV	Coefficient of Variation
FIS	Fuzzy Inference Systems
LSE	Least Squares Estimation
MAE	Mean Absolute Error
MAPE	Mean Absolute Percentage Error
PCT	Parallelization Control Technique
PID	Proportional Integral Derivative
PV	Photovoltaic
RMSE	Root Mean Squared Error

II. MATERIAL AND METHODS

A. TETRAHEDRON SENSOR



FIGURE 1. Tetrahedron sensor

The tetrahedron sensor is a type of sensor used to detect the position of sunlight. This sensor has a pyramid shape with three sides, each equipped with a light sensor in the form of a phototransistor. Figure 1 shows a phototransistor in the center of each side of the pyramid, with each position labelled P_1 , P_2 , and P_3 . The sensor has a height of 10 cm and a base length of 5 cm. The type of light sensor and the dimensions of the tetrahedron are based on previous studies [22], [23]. The tetrahedron sensor operates on the principle of comparing values from each phototransistor. Based on these comparisons, the sensor can determine the sun's position regarding azimuth and altitude.

B. ADAPTIVE NEURO-FUZZY INFERENCE SYSTEM

ANFIS is a hybrid intelligent system that combines the strengths of fuzzy logic and ANN. Fuzzy logic provides a reasoning approach that mimics human thinking and can handle uncertainty and ambiguity. At the same time, ANN can learn from data and recognize complex patterns [53], [54]. The ANFIS architecture consists of several layers, each responsible for specific operations. The first layer performs fuzzification, where membership functions map input values to fuzzy sets. The second layer is the rule layer, where the firing strength of fuzzy rules is calculated. The third layer normalizes the firing strengths, while the fourth layer generates the output by multiplying the normalized firing strength with the consequent part of the fuzzy rules. Finally, the output layer combines these results to produce the final output [55].



FIGURE 2. The architecture of ANFIS network

ANFIS is trained to optimize fuzzy parameters through a learning method that combines the concepts of ANN and fuzzy. The training starts by determining the initial structure of ANFIS, including fuzzy rules, membership functions, and rule types [56]. Training data guides the training process, where the system updates the membership function and consequent parameters [57]. The training process typically consists of two phases: forward pass and backward pass. In the first process, the forward pass, input is fed into ANFIS, and the output is computed through the fuzzy inference mechanism. including fuzzification, firing strength calculation, normalization, and defuzzification to produce the final output [58]. The proposed ANFIS network structure in this study is shown in Figure 2. The first layer is the fuzzification layer, where each node in this layer calculates the membership degree of each input based on the corresponding membership function. The membership function of each input can be calculated using the following equation [59],

$$\mu_i(x_i) = f_i(x_i) \tag{1}$$

where, $\mu_j(x_i)$ is the membership degree for input x_i in the fuzzy set *j* and $f_i(x_i)$ is the membership function of input x_i



in the fuzzy set j. In this study, a Gaussian Membership Function is used, which is expressed in the following equation,

$$f(x) = gaussian(x; c, \sigma) = e^{-\frac{1}{2}\left(\frac{x-c}{\sigma}\right)^2}$$
(2)

where, *c* is the mean value that serves as the center of the membership function, and σ is the standard deviation that determines the width of the membership function.

The second layer is the rule layer, where each node represents the firing strength for each fuzzy rule formed based on the combination of membership functions for each input. The firing strength is calculated as the product of the input signals that represent the premises in the fuzzy rules, as expressed in the following equation,

$$w_i = \prod_{i=1}^{3} \mu_j(x_i)$$
 (3)

where, w_i represents the output firing strength for rule *i*. Then, the firing strength values are normalized in the third layer, the normalization layer. This process ensures that the relative contribution of each fuzzy rule is correctly accounted for so that the total firing strength of all rules equals 1. The normalization process is performed using the following equation,

$$\overline{w_i} = \frac{w_i}{\sum_{i=1}^N w_i} \tag{4}$$

where, $\overline{w_i}$ represents the normalized firing strength and *N* is the number of fuzzy rules. Next, in the fourth layer, the defuzzification layer, each node multiplies the normalized firing strength by the output of the consequent fuzzy rule using the following equation,

$$z_i = \overline{w_i} \,.\, f(x_i) \tag{5}$$

where, z_i represents the defuzzified output for input x_i and $f(x_i)$ represents the output of the consequent rule for rule *i*. The consequent rule is a mathematical expression that determines the fuzzy output based on the input and the existing rules.

Next, in the fifth layer is the output layer. In this layer, each node combines all the signals received from the previous layers to produce the final output of the ANFIS, as expressed by the following equation,

$$y = \sum_{i=1}^{N} z_i \tag{6}$$

The consequent parameters are updated using the Least Squares Estimation (LSE) method by calculating the error between the system output y and the target output y_t , based on the total dataset m. The error is defined as follows,

$$E = \frac{1}{2} \sum_{i=1}^{m} (y_i - y_{t,i})^2 \tag{7}$$

After that, in the second process, the backward pass is performed using the backpropagation method to minimize the error by updating the parameters c and σ of the membership function based on the calculated error. To update the parameter c, the following equation is used,

$$c_{new} = c_{old} - \eta \frac{\partial E}{\partial c} \tag{8}$$

where, $\frac{\partial E}{\partial c}$ is the partial derivative of the error concerning *c* and η is the learning rate. Then, to update the parameter σ , the following equation is used,

$$\sigma_{new} = \sigma_{old} - \eta \frac{\partial E}{\partial \sigma} \tag{9}$$

where, $\frac{\partial E}{\partial \sigma}$ is the partial derivative of the error concerning σ . This process is repeated until the error reaches a minimum value or until a certain number of iterations is reached.



FIGURE 3. Proposed triple-axis sun tracker

C. SUN TRACKER SYSTEM

Figure 3 shows the physical device of the sun tracker system. The proposed design implements a triple-axis mechanism with three manipulator arms. This mechanism allows the system to follow the sun's position more quickly as the motors move in parallel. The system uses servo motors as its actuators.



FIGURE 4. The movement of sun's position



In the testing process, the sun tracker system is compared with the sun's movement path to evaluate the performance of the proposed system. Figure 4 illustrates the position of the sun relative to the tracker. Two main parameters are used to determine the sun's position: azimuth and altitude. Azimuth is the horizontal angle measured clockwise from the north. An angle of 90° means the sun is in the east, 180° in the south, and 270° in the west. Azimuth indicates the sun's direction along the horizon [60]. Meanwhile, altitude measures the sun's height above the horizon, calculated from the horizontal line to the sun's position. This angle changes throughout the day, starting at 0° when the sun rises, reaching its peak at noon, and then returning to 0° when the sun sets [61]. The sun's movement path can be calculated using astronomical formulas based on location and time. The equation to calculate the solar azimuth angle (ϕ_s) is expressed as follows,

$$\sin \phi_S = \frac{\cos \delta \, . \sin \gamma_H}{\cos \varphi_S} \tag{10}$$

where, δ is the solar declination angle, which can be calculated using the following equation,

$$\delta = 23.45^{\circ} . \sin\left(360 . \frac{284 + n}{365}\right) \tag{11}$$

where, *n* is the day number in the year. Meanwhile, γ_H is the solar hour angle, expressed as follows,

$$\gamma_H = 15^{\circ} \left(T_r - 12 \right) \tag{12}$$

where, T_r is the true time, ranging from 0 to 24 hours. Then, φ_s is the solar altitude angle, expressed as follows,

$$\sin \varphi_S = \sin \omega \, . \, \sin \delta + \cos \omega \, . \, \cos \delta \, . \, \cos \gamma_H \qquad (13)$$

where, ω represents the latitude coordinate based on the location on earth.

III. PROPOSED METHOD

The proposed method includes ANFIS modelling and determining the most optimal consequent rule to be applied. It also explains the proposed mechanical structure in the sun tracker system, which aims to optimize the movement of the solar panels to enhance solar energy absorption efficiency. The modeling process of ANFIS and the simulation of the sun tracker system were conducted on a computer with an AMD Ryzen 5 4600H CPU, 16 GB DDR4 RAM, and an NVIDIA GeForce GTX 1650 Ti GPU with 4 GB memory. Additionally, the software used includes Python 3.10 with TensorFlow version 2.12.0. The flowchart illustrating the entire proposed system, including the ANFIS modeling method and sun tracker control, is shown in Figure 5.

A. ANFIS MODEL

In this study, ANFIS is used to control the movement of servo motors based on the light intensity readings from the

tetrahedron sensor. The rotation of the motors affects the movement of the manipulator arms, which direct the PV towards the sun. This study proposes ANFIS-PCT, consisting of three ANFIS models, each responsible for controlling a different motor, as shown in Figure 6, with the structure of each network shown in Table 3. The proposed membership function utilizes a Gaussian function chosen for its flexibility in modeling nonlinear relationships between inputs and outputs [62]. The number of membership functions for each input was determined based on performance evaluation through simulation, where three membership functions per input demonstrated a balance between computational complexity and model accuracy. Using more than three membership functions increases accuracy but significantly adds to computation time, making it unsuitable for real-time sun tracker systems. The learning rate parameter was set to 0.01 after testing, which showed that this value provides stable convergence without compromising training speed. Additionally, the number of training iterations was set to 5000 epochs based on observations indicating that the model achieves minimum error performance within this range.

TABLE 3. Proposed ANFIS structure

Parameter	Value	Description
Number of input	3	Number of nodes in the input layer
Number of output	1	Number of nodes in the output layer
Number of fuzzy MF 1	3	Number of membership functions at input node 1
Number of fuzzy MF 2	3	Number of membership functions at input node 2
Number of fuzzy MF 3	3	Number of membership functions at input node 3
Membership function	Gaussian function	Membership function at input
Number of rules	27	Number of rules fuzzy
Number of datasets	1945	Number of data for training process
Learning rate	0.01	ANFIS learning rate parameter

Based on Figure 6, ANFIS 1 model controls the angle (θ) of servo motor 1 based on inputs from P_1 sensor, P_2 sensor, and the initial angle (θ_0) of servo motor 1. ANFIS 2 model controls the angle of servo motor 2 based on inputs from P_2 sensor, P_3 sensor, and the initial angle of servo motor 2. Meanwhile, ANFIS 3 model controls the angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3. Next, the output angle of each motor is calculated and used to move the three arms of the sun tracker.

There is a consequent rule in defuzzification, obtaining results based on fuzzy rules by describing the mathematical relationship between input and output [63]. The parameters in the consequent rule are optimized during the training process to ensure that the model can accurately predict the output based on the given data. This paper proposes three





FIGURE 5. Flowchart of ANFIS modeling and solar tracking control system

types of consequent rules: polynomial functions of firstorder, second-order, and third-order. These consequent rules are applied to Eq. (5). The first-order function is expressed as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + r \tag{14}$$

where, $f(x_i)$ represents the output of the consequent rule, p_i is the first-order parameter for input x_i , and r is the bias constant of the rule. Meanwhile, for the second-order function, the equation is as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + \sum_{i=1}^{3} q_i x_i^2 + \sum_{1 \le i < k \le 3} c_{i,k} x_i x_k + r \quad (15)$$

where, q_i is the second-order parameter for input x_i and $c_{i,k}$ is the parameter for the cross terms between inputs x_i and x_k . Then, for the third-order function, the equation is as follows,

$$f(x_i) = \sum_{\substack{i=1\\3}}^{3} p_i x_i + \sum_{\substack{i=1\\3}}^{3} q_i x_i^2 + \sum_{\substack{1 \le i < k \le 3\\1 \le i < k \le 3}} c_{i,k} x_i x_k + \sum_{\substack{i=1\\i=1}}^{3} t_i x_i^3 + r$$
(16)

where, t_i is the second-order parameter for input x_i .

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B. MECHANICAL STRUCTURE OF SUN TRACKER

This sun tracker system configuration uses three manipulator arms, as shown in Figure 7. The model of the manipulator arms is arranged in a parallel configuration, with servo motors as the actuators. These three arms are connected to a triangular plane that serves as the base for the PV. Points J_1 , J_2 , and J_3 connect the plane to the manipulator arms. The height of these points will affect the orientation of the PV in following the sun's movement.



FIGURE 7. Triple-arm manipulator configuration on sun tracker system



FIGURE 8. The configuration of arm manipulator: (a) arm structure design, (b) system mechanism

The configuration of the manipulator arm is shown in Figure 8(a). The arm consists of the upper arm (b_i) and the lower arm (a_i) , with lengths of 3.7 cm and 1.6 cm, respectively. Additionally, there are two connection points: the elbow point (E_i) and the end-effector point (J_i) , as well as a drive point M_i as the motor (for i = 1,2,3). The E_i point is the connection between the lower and upper arm, while J_i is the connection between the upper arm and the base plane where the PV is mounted. Figure 8(b) shows the drive mechanism of the manipulator arm. The angle β_i is the orientation angle of the manipulator arm relative to the *x*-axis. The movement of motor M_i will create an angle θ_i . This angle



will affect the value of angle α_i at point E_i , causing the coordinates at point J_i to change. These coordinate changes can be calculated using the following forward kinematic equation [64], [65],

$$J_i x = (a_i \cos \theta_i + b_i \cos(\theta_i + \alpha_i)) \cos \beta_i + M_i x \quad (17)$$

$$J_i y = (a_i \cdot \cos \theta_i + b_i \cdot \cos(\theta_i + \alpha_i)) \sin \beta_i + M_i y \quad (18)$$

$$J_i z = a_i . \sin \theta_i + b_i . \sin(\theta_i + \alpha_i) + M_i z$$
(19)

By applying trigonometric theorems, we obtain,

$$J_{i}x = (a_{i} \cdot \cos \theta_{i} + b_{i}(\cos \theta_{i} \cdot \cos \alpha_{i} - \sin \theta_{i} \cdot \sin \alpha_{i}))$$

$$cos \beta_{i} + M_{i}x$$

$$(20)$$

$$J_{i}y = (a_{i} \cdot \cos \theta_{i} + b_{i}(\cos \theta_{i} \cdot \cos \alpha_{i} - \sin \theta_{i} \cdot \sin \alpha_{i}))$$

$$sin \beta_{i} + M_{i}y$$

$$(21)$$

$$J_{i}z = (a_{i} \cdot \sin \theta_{i} + b_{i}(\sin \theta_{i} \cdot \cos \alpha_{i} + \cos \theta_{i} \cdot \sin \alpha_{i}))$$

$$+M_{i}z$$

$$(22)$$

In this condition, the arm b_i remains perpendicular at 90° to the base, even when motor M_i moves. This is because point J_i is connected to the triangular plane above it, keeping arm b_i perpendicular. The simulation of this movement is shown in Figure 9. Based on this condition, the angle $\alpha_i = 90 + \theta_i$, so by applying the rules $cos(90 + \theta_1) = -sin \theta_i$ and $sin(90 + \theta_1) = cos \theta_i$, we obtain $sin \alpha_i = cos \theta_i$ and $cos \alpha_i = -sin \theta_i$. Then, by substituting in Eq. (20), Eq. (21), and Eq. (22), the following equations is derived.

For the point x,

$$J_{i}x = (a_{i} \cdot \cos \theta_{i} + b_{i}(-\cos \theta_{i} \cdot \sin \theta_{i} - \sin \theta_{i} \cdot \cos \theta_{i})$$

$$\cos \beta_{i} + M_{i}x$$

$$(23)$$

$$J_{i}x = (a_{i} \cdot \cos \theta_{i} + b_{i}(-2\sin \theta_{i} \cdot \cos \theta_{i})\cos \beta_{i} + M_{i}x$$

$$J_{i}x = (a_{i} \cdot \cos \theta_{i} + b_{i} \cdot \sin 2\theta_{i}) \cdot \cos \beta_{i} + M_{i}x$$

$$(25)$$

For the point y,

$$J_{i}y = (a_{i}.\cos\theta_{i} + b_{i}(-\cos\theta_{i}.\sin\theta_{i} - \sin\theta_{i}.\cos\theta_{i})$$

$$\sin\beta_{i} + M_{i}y$$
(26)

$$J_i y = (a_i \cdot \cos \theta_i + b_i (-2\sin \theta_i \cdot \cos \theta_i) \sin \beta_i + M_i y$$
(27)
$$I_i y = (a_i \cdot \cos \theta_i + b_i \sin 2\theta_i) \sin \beta_i + M_i y$$
(28)

For the point z,

$J_i z = (a_i \cdot \sin \theta_i + b_i (-\sin \theta_i \cdot \sin \theta_i + \cos \theta_i \cdot \cos \theta_i)$	
$+M_i z$	<mark>(29)</mark>
$J_i z = (a_i . \sin \theta_i + b_i (1 - 2 \sin^2 \theta_i) + M_i z$	<mark>(30)</mark>
$J_i z = a_i . \sin \theta_i + b_i . \cos 2\theta_i + M_i z$	<mark>(31)</mark>

In the proposed system, the angle β_i varies for each motor. In Figure 10(a), the top view shows the orientation of motors M_1 , M_2 , and M_3 , each connected to arms a_1 , a_2 , and a_3 at points E_1 , E_2 , and E_3 . The angle between each motor is depicted, with 315° for M_1 , 45° for M_2 , and 180° for M_3 . Meanwhile, Figure 10(b) shows the physical layout or placement positions of the motors and the manipulator arms connected at the same points. These motors are strategically positioned to move each arm accurately.



FIGURE 9. Principle work of manipulator arm movement: (a) downward movement, (b) upward movement



FIGURE 10. The arrangement of servo motors from a top view: (a) orientation of each motor, (b) position of each motor



FIGURE 11. The normal vector on the triangular plane



Next, the tracker system's azimuth and altitude direction are calculated based on each motor's movement angle. To determine these values, it is necessary to calculate the normal vector of the triangular plane, as shown in Figure 11, where $\vec{v_0}$ is the initial normal vector when its direction is perpendicular upward, and \vec{v} is the normal vector when its direction changes. Based on the coordinate points $J_1(x_1, y_1, z_1), J_2(x_2, y_2, z_2)$, and $J_3(x_3, y_3, z_3)$, the normal vector is calculated using the following equation,

$$\vec{v} = \vec{J_1 J_2} \cdot \vec{J_1 J_3} \tag{32}$$

where, $\overline{J_1J_2}$ is the vector from point J_1 to point J_2 and $\overline{J_1J_3}$ is the vector from point J_1 to point J_3 . The vectors in Eq. (32) can be calculated using the following equations,

$$\overrightarrow{J_1J_2} = (x_2 - x_1, y_2 - y_1, z_2 - z_1)$$
(33)

$$\overrightarrow{J_1J_3} = (x_3 - x_1, y_3 - y_1, z_3 - z_1)$$
(34)

Thus, from Eq. (33) and Eq. (34), the normal vector is expressed as follows,

$$\vec{v} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ x_2 - x_1 & y_2 - y_1 & z_2 - z_1 \\ x_3 - x_1 & y_3 - y_1 & z_3 - z_1 \end{vmatrix}$$
(35)

So that, we obtain,

$$y_x = (y_2 - y_1)(z_3 - z_1) - (y_3 - y_1)(z_2 - z_1)$$
 (36)

$$v_y = (x_2 - x_1)(z_3 - z_1) - (x_3 - x_1)(z_2 - z_1)$$
(37)

$$v_z = (x_2 - x_1)(y_3 - y_1) - (x_3 - x_1)(y_2 - y_1)$$
 (38)

Based on Eq. (36), Eq. (37), and Eq. (38), the tilt angle of the plane concerning the x-axis (θ_x) and the y-axis (θ_x) can be determined using the following equations,

$$\theta_x = \cos^{-1}\left(\frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}}\right)$$
(39)

$$\theta_{y} = \cos^{-1} \left(\frac{v_{y}}{\sqrt{v_{x}^{2} + v_{y}^{2} + v_{z}^{2}}} \right)$$
(40)

Meanwhile, to calculate the tracker azimuth (ϕ_T) and tracker altitude (φ_T), the following equations are used,

$$\phi_T = tan^{-1} \left(\frac{v_y}{v_x} \right) \tag{41}$$

$$\varphi_T = tan^{-1} \left(\frac{v_z}{\sqrt{v_x^2 + v_y^2}} \right) \tag{42}$$

Meanwhile, point G is the centroid of the triangle and can be calculated using the following equation,

$$\begin{bmatrix} G_x \\ G_y \\ G_z \end{bmatrix} = \begin{bmatrix} (x_1 + x_2 + x_3)/3 \\ (y_1 + y_2 + y_3)/3 \\ (z_1 + z_2 + z_3)/3 \end{bmatrix}$$
(43)

IV. PERFORMANCE ANALYSIS

The analysis provides performance results of each model in predicting PV output power based on its operational temperature. The analytical methods used include calculating Mean Absolute Error (MAE), Root Mean Squared Error (RMSE), Mean Absolute Percentage Error (MAPE), Coefficient of Determination (R^2), and Coefficient of Variation (CV).

MAE is one of the commonly used methods to analyze model performance. It measures the average absolute difference between the predicted values generated by the model and the actual values in the test data. This result shows how closely the model predictions match the actual values overall. The equation for MAE is as follows,

$$MAE = \frac{1}{n} \sum_{i=n}^{n} |y_i - \hat{y}_i|$$
(44)

where, *n* is the number of test data points, y_i is the actual value, and \hat{y}_i is the value predicted by the model for the *i* data point. A lower MAE value indicates better model performance, signifying that the model's predictions are closer to the actual values [66]. Next, RMSE analysis is conducted by calculating the square root of the average of the squared differences between the model's predicted values and the actual values. The equation for RMSE is defined as follows,

$$RMSE = \sqrt{\frac{1}{n} \sum_{i=n}^{n} (y_i - \hat{y}_i)^2}$$
(45)

RMSE analysis indicates the average deviation between the model's predicted and actual values. By taking the square root, RMSE offers a more intuitive interpretation in the same units as the target variable. A lower RMSE value indicates better model performance, meaning the model's predictions are closer to the actual values [67]. Next, MAPE analysis is a method to measure the error rate of a model by calculating the average of the absolute percentage error between the predicted and actual values. The equation for calculating MAPE is defined as follows,

$$MAPE = \frac{1}{n} \sum_{i=n}^{n} \left| \frac{y_i - \hat{y}_i}{y_i} \right| .100\%$$
(46)

The MAPE value indicates the prediction error in percentage terms. The lower the MAPE value, the better the model's performance in predicting the data. One advantage of MAPE is its ease of interpretation, as the result is a percentage. Next, the R^2 analysis, known as the Coefficient of Determination, is used to measure how well the developed model can explain the variability in the data. The equation for the Coefficient of Determination is defined as follows,

$$R^{2} = 1 - \frac{\sum_{i=1}^{n} (y_{i} - \hat{y}_{i})^{2}}{\sum_{i=1}^{n} (y_{i} - \hat{y})^{2}}$$
(47)

where, \hat{y} is the mean of all y_i values. The R^2 value ranges from 0 to 1, where a value closer to 1 indicates that the model better explains the variability in the data. R^2 analysis can determine how much output data variability can be explained by the input data. Lastly, the CV analysis, or Coefficient of Variation, is a statistical measure to assess a dataset's relative degree of variation. CV is defined as the ratio of the standard deviation to the mean, expressed as follows,

$$CoV = \frac{\sqrt{\frac{1}{n}\sum_{i=1}^{n} \left(y_{i} - \frac{1}{n}\sum_{i=1}^{n} y_{i}\right)^{2}}}{\frac{1}{n}\sum_{i=1}^{n} y_{i}}$$
(48)

CV is typically used to measure data stability. A low CV value indicates more stable data, while a high CV value suggests more significant variability in the data.

V. RESULTS AND DISCUSSION

In this section, an evaluation is conducted to assess the performance of ANFIS in each model based on the type of consequent rule. Then, the movement of the three motors is simulated to obtain the azimuth and altitude angles. Testing uses the sun tracker device to assess the system's ability to track the sun's position. Finally, comparing previous systems is necessary to validate the proposed sun tracker system's effectiveness.

A. MODEL PERFORMANCE ANALYSIS

Table 4 presents the statistical results from the model's training and testing phases based on three types of consequent rules: first-order, second-order, and third-order. The dataset consists of 80% for training and 20% for testing. The ANFIS training and testing results show that the choice of consequent rule significantly impacts each model's performance.







FIGURE 12. The comparison analysis of consequence rule variations to controlling motor movements (a) ANFIS 1 model, (b) ANFIS 2 model, (c) ANFIS 3 model

In ANFIS model 1, the second-order performed best compared to the first-order and third-order, both in the training and testing phases. During training, the second-order achieved the lowest MAE, RMSE, and MAPE values, at 3.6, 4.5, and 8.08%, respectively, along with a high R^2 value of 0.98. This result indicates that the model can predict motor movement accurately based on the input data. In testing, the second-order also excelled with the lowest MAE, RMSE, and MAPE values, at 2.82, 3.34, and 7.02%, respectively, indicating accurate model performance with minimal error. In ANFIS model 2, a similar pattern emerged, with the secondorder demonstrating optimal performance. During training, the second-order model yielded low MAE, RMSE, and MAPE values of 3.82, 4.74, and 8.3%, along with a high R^2 value of 0.97. In testing, the second-order produced MAE, RMSE, and MAPE values of 3, 3.58, and 6.44%, respectively, outperforming the first-order and third-order models. In ANFIS model 3, the second-order also provided the best results, achieving the lowest error values in training with MAE, RMSE, and MAPE of 3.8, 4.68, and 7.69%, respectively, and the highest R^2 value of 0.98. However, in testing, the second-order's performance was less optimal than the third-order, as indicated by higher MAE, RMSE, and MAPE values than the third-order. The training and testing



analysis results show that the second-order consequent rule is optimal for all three ANFIS models.



FIGURE 13. The relationship between the phototransistor ratio values with the motor angle increases based on various consequent rules: (a) first-order, (b) second-order, and (c) third-order

Figure 12(a) displays the motor movement results with different consequent rules. The graph shows that all three consequent rules follow the angle change patterns quite well, although first-order shows more significant discrepancies. Meanwhile, in Figure 12(b), the first-order consequent rule exhibits noticeable differences, especially in the sixth and eighth experiments. On the other hand, second-order and third-order are more consistent in approaching the actual

angle, although slight differences still exist at some points. In Figure 12(c), the average difference between the actual angle and the angle produced by each consequent rule is more minor than the previous graph. Overall, although both second-order and third-order consequent rules accurately follow the angle change patterns of all three motors, there are some points where the second-order performs better than the third-order. Figure 13 shows a three-dimensional graph illustrating the relationship between the ratio of two phototransistor values and the output as the motor angle increments for each consequent rule. The comparison values from the two phototransistor readings directly affect the magnitude of the resulting angle increment. In the first-order consequent, the angle increment pattern appears linear. In the second-order consequent, a significant angle increment occurs with more considerable phototransistor ratio differences; the greater the difference, the higher the angle increment. Conversely, there is no considerable angle increase for ratios closer in value. In the third-order, the angle increment pattern is similar to the second-order but displays fluctuations or a nonlinear pattern in the middle of the graph. This indicates that there are points where small changes in the phototransistor ratio can lead to a lower or even decreasing angle increment.



FIGURE 14. The simulation of azimuth and altitude changes based on motor movement ($M_1 = 26^\circ, M_2 = 40^\circ, M_3 = -30^\circ$)

After obtaining the model, a motor movement simulation was conducted on the sun tracker to observe the relationship between the movements of the three motors and changes in azimuth and altitude angles. Figure 14 displays the simulation results, showing how each motor's activity influences the panel's orientation changes. In this simulation, it demonstrates the condition where the three motors move at angles $M_1 = 26^\circ$, $M_1 = 40^\circ$, and $M_1 = -30^\circ$, resulting in a normal vector direction of (0, 8, 26) with tilt angles of $\theta_x = 90^\circ$ and $\theta_y = 72^\circ$. Meanwhile, the resulting azimuth and altitude angles are 89° and 72°, respectively. Further testing



Madal	Demonster	Training			Testing			
Model	Parameter	First-Order	Second-Order	Third-Order	First-Order	Second-Order	Third-Order	
	MAE	9.3	3.6	5.26	9.57	2.82	4.08	
	RMSE	11.61	4.5	6.21	11.33	3.34	4.95	
ANFIS 1	MAPE	21.79%	8.08%	17.08%	21.78%	7.02%	10.5%	
	\mathbb{R}^2	0.81	0.98	0.96	0.83	0.99	0.97	
	CV	0.39	0.49	0.47	0.42	0.47	0.44	
	MAE	11.09	3.82	5.08	9.79	3	3.51	
	RMSE	13.78	4.74	6.05	11.81	3.58	4.33	
ANFIS 2	MAPE	19.44%	8.3%	12.86%	21.57%	6.44%	8.79%	
	\mathbb{R}^2	0.69	0.97	0.95	0.82	0.99	0.98	
	CV	0.3	0.42	0.4	0.4	0.46	0.46	
	MAE	11.76	3.8	4.41	8.94	2.86	2.77	
	RMSE	14.1	4.68	5.33	10.86	3.48	3.4	
ANFIS 3	MAPE	22.83%	7.69%	8.83%	18.52%	6.35%	6.11%	
	R ²	0.7	0.98	0.97	0.85	0.99	0.99	
	CV	0.35	0.48	0.43	0.41	0.47	0.47	

TABLE 4. The results of ANFIS training and testing with various consequent rules



FIGURE 15. The results of the sun tracker movement experiment based on all combinations of angles M_1 , M_2 , and M_3 : (a) azimuth angle movement and (b) altitude angle movement

results are shown in Figure 15, combining an angle range of -30° to 90°, representing the minimum to maximum motor angles. Figure 15(a) shows that the azimuth angle ranges from 0° to 360°, while Figure 15(b) indicates that the altitude angle ranges from 60° to 90°. This angle range demonstrates that the

triple-axis mechanism can achieve good orientation flexibility, allowing the system to adjust the PV panel position effectively to minimize the solar incidence angle.

Subsequent testing was conducted to analyze the response of the sun tracker system in mitigating uncertain disturbances, such as the continuous movement of light due to cloud movement or shadows from external objects. The testing scenario involved observing the movement of the sun tracker at azimuth and altitude angles of 89° and 72°, respectively. The results of the sun tracker system's response based on ANFIS consequent rules are shown in Figure 16. Based on these tests, the proposed control rules were able to mitigate the effects of disturbances, such as changes in light intensity due to clouds, while maintaining the optimal orientation of the solar panel. Under partial shading conditions, where some sensors or PV panels receive reduced light intensity due to shadows from clouds or surrounding objects, the tracking system may face challenges in maintaining the optimal orientation of the solar panel toward the sun.





FIGURE 16. The comparison result of responses to light changes for each ANFIS consequent rules (a) azimuth movement, (b) altitude movement

Further analysis was conducted to determine the system's response to each ANFIS consequent rule in response to changes in light position. The study was performed by comparing the system's response based on Figure 16. This analysis considered characteristics such as rise time, peak time, overshoot, settling time, and steady-state error for both azimuth and altitude movements, which are presented in Table 5 and Table 6. For azimuth movement, second-order showed the most optimal performance, achieving the fastest rise time and settling time with low steady-state error. The second-order response also did not exhibit any overshoot. Meanwhile, the peak time obtained was longer than that of the first-order. In the first-order, the settling time was unavailable because the system response did not reach a steady-state condition during the observation period. For altitude movement, the analysis also indicated that the second-order performed better than the others. No overshoot occurred in the second-order, as with the azimuth movement. In the first-order, the settling time was also unavailable, as the system response did not reach a steady-state condition. This analysis reveals that second-order is the best choice for controlling both azimuth and altitude movements, making this consequent rule most suitable for implementation in ANFIS-PCT for a triple-axis sun tracker system.

TABLE 5. The comparison of performance ANFIS consequent rules on azimuth movement

Parameter	First-order	Second-order	Third-order
Rise Time (s)	<mark>0.681</mark>	<mark>0.601</mark>	<mark>0.661</mark>
Peak Time (s)	<mark>1.403</mark>	<mark>1.723</mark>	<mark>1.483</mark>
Overshoot (%)	<mark>0.899</mark>	<mark>0</mark>	<mark>0.562</mark>
Settling Time	-	<mark>1.462</mark>	<mark>2.212</mark>
Steady State Error	0.679	0.03	0.111

 TABLE 6. The comparison of performance ANFIS consequent rules on altitude movement

Parameter	<mark>First-order</mark>	<mark>Second-order</mark>	Third-order
Rise Time (s)	0.511	<mark>0.491</mark>	0.521
Peak Time (s)	<mark>2.685</mark>	<mark>1.493</mark>	<mark>1.283</mark>
Overshoot (%)	<mark>0.556</mark>	<mark>0</mark>	<mark>0.139</mark>
Settling Time	-	<mark>1.34</mark>	<mark>1.538</mark>
Steady State Error	<mark>0.399</mark>	0.027	0.213

B. SUN TRACKER SYSTEM PERFORMANCE ANALYSIS Figure 17(a) compares the sun tracker movement and the azimuth angle of the actual sun position. The graph shows the sun tracker accurately follows the sun's azimuth angle from sunrise to sunset. Meanwhile, Figure 17(b) compares the altitude angle. Based on this graph, a discrepancy occurs at the start of tracking, around 7:00 AM to 8:00 AM. Then, the sun tracker successfully tracks the sun's altitude more accurately, reaching a peak at 12:30 PM at its maximum altitude. Afterwards, the altitude of the sun tracker gradually decreases in sync with the sun's position until sunset. Overall, the sun tracker system works effectively to adjust its movement in tracking the sun's position in azimuth and altitude angles, thereby minimizing the solar incidence angle on the PV surface throughout the day.



FIGURE 17. The result comparison between the tracked and the sun's actual position: (a) azimuth movement and (b) altitude movement

C. SYSTEM PERFORMANCE COMPARISON

Table 7 compares the proposed ANFIS model's performance with several previous models related to sun tracker systems. The comparison aims to validate the performance of the proposed ANFIS model in tracking the sun's position. The models compared include PID-ANN [44], Fast Integral Terminal Sliding Mode Control (FIT-SMC) [68], Neural Network Algorithm with Model Predictive Control (NNA-MPC) [69], PID with Internal Model Controller (PID-IMC) [51], PID with Fuzzy Logic Controller (PID-FLC) [48], PD with Fuzzy Logic Controller (PD-FLC) [46], and Artificial Bee Colony (ABC) [50]. The parameters compared are rise time, settling time, and steady-state error. Based on the comparison, the proposed ANFIS-PCT model demonstrates optimal performance. For the rise time parameter, ANFIS-PCT has a relatively fast time, only behind the FIT-SMC model, which recorded the most rapid rise time of 0.15 seconds. However, compared to other models,



ANFIS-PCT is far superior. For the settling time parameter, ANFIS-PCT also shows optimal performance, although it is still behind FIT-SMC, which recorded the fastest time. Meanwhile, for the steady-state error, ANFIS-PCT demonstrates a more stable and accurate system.

TABLE 7. The comparison of the proposed ANFIS model with other published models

Model	<mark>Rise Time</mark> (s)	<mark>Settling Time</mark> (s)	<mark>Steady State</mark> Error
ANFIS-PCT (Proposed)	<mark>0.55</mark>	<mark>1.4</mark>	<mark>0.03</mark>
PID-ANN	<mark>2.18</mark>	<mark>2.46</mark>	<mark>0.07</mark>
FIT-SMC	<mark>0.15</mark>	<mark>0.33</mark>	-
NNA-MPC	-	<mark>0.108</mark>	-
PID-IMC	<mark>1.8</mark>	<mark>5.58</mark>	-
PID-FLC	<mark>3.6</mark>	<mark>4.8</mark>	<mark>0.4</mark>
PD-FLC	<mark>6.38</mark>	<mark>6.38</mark>	0.83
ABC	<mark>2.37</mark>	5.23	1.05

VI. CONCLUSION

Based on the analysis results, all three proposed ANFIS models using the second-order consequent rule deliver the best performance compared to the first-order and third-order, both in the training and testing phases. The simulation results show that the movement of the sun tracker with a triple-axis mechanism can reach an azimuth angle ranging from 0° to 360°. In contrast, the altitude angle ranges from 60° to 90°. These values indicate that the sun tracker has good flexibility. The proposed system has nonlinear dynamics, so several parameters must be continuously optimized through the training process to gradually reduce the error value in the system until it approaches zero. This indicates that the system will always move towards stability, even with small variations in input parameters or disturbances.

Although the proposed sun tracker system offers improved accuracy and responsiveness in tracking the sun's position, it has some drawbacks, including system complexity, leading to higher energy consumption. This is due to the number of motors that need to move simultaneously to reach the optimal position. The additional energy the motors consume in the triple-axis mechanism can reduce overall energy efficiency, especially in conditions with limited energy sources.

Future research will focus on developing triple-axis sun tracker technology techniques to enhance efficiency by reducing energy consumption and optimizing PCT in ANFIS to make it more adaptive in tracking the sun's position. Further research can be developed by exploring the Lyapunov method to explicitly determine the stability of the sun tracker system, allowing the mathematical proof to support the experimental results that have been conducted. Additionally, future research will focus on exploring energy-saving strategies, including optimizing by reducing unnecessary servo motor movements, as well as evaluating the comparison between the energy produced and the total energy consumed.

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Original Article Title: "ANFIS Parallelization Control on Triple-Axis Sun Tracker to Minimize Solar Rays Incidence Angle on Photovoltaic"

To: IEEE Access Editor

Re: Response to reviewers

Dear Editor,

Thank you for allowing a resubmission of our manuscript, with an opportunity to address the reviewers' comments.

We are uploading (a) our point-by-point response to the comments (below) (response to reviewers, under "Author's Response Files"), (b) an updated manuscript with yellow highlighting indicating changes (as "Highlighted PDF"), and (c) a clean updated manuscript without highlights ("Main Manuscript").

Best regards,

Yuwaldi Away et al.

Reviewer#1, Concern #1: The introduction needs to be enhanced. Although authors have incorporated many literatures, the writing stays at a superficial level. It is important to demonstrate the challenge of the research investigated and the gap closed by the proposed work. More explicitly, the novelty and contribution of the proposed work are not well demonstrated.

Author response: We thank the reviewer for making this suggestion. We have added for this point at the section "Introduction", paragraphs 5-6, on pages 3-4, specifically marked with a yellow highlight.

Author action: We have updated the manuscript about investigating the gap in the proposed work by adding the following explanation:

"Based on these studies, most current sun tracker systems still rely on single-axis or dual-axis mechanisms, which have limitations in vertical adjustments and in avoiding shadows from objects surrounding the panels. On the other hand, research on triple-axis mechanisms is still minimal. Additionally, optimization techniques are needed to enhance the performance of the ANFIS algorithm in managing the complexity of sun tracker systems, particularly in triple-axis mechanisms. As a solution, the sun tracker system with a triple-axis drive mechanism is proposed."

"ANFIS-PCT offers an optimal balance between computational complexity, robustness against nonlinearity, and real-time responsiveness, making it the best solution for triple-axis sun tracker systems"

We also have updated the contribution of the proposed work by adding the following explanation:

"The novelty of this research lies in the implementation of PCT in ANFIS, which enables the division of computational processes into multiple parts running concurrently. Additionally, this study analyzes various consequent rule configurations in the ANFIS model, including first-order, second-order, and third-order polynomial functions, to determine the most optimal configuration. The main contributions of this paper are as follows:

- We propose a sun tracker system using a triple-axis mechanism consisting of three manipulator arms to control the azimuth and altitude angles. This system enables PV panels to adjust their angles optimally to the direction of incoming sunlight.
- We propose an ANFIS algorithm with PCT to control the movement of the sun tracker through separate control processes, making the system more responsive and accurate.
- We demonstrate that the second-order consequent rule provides the best performance in controlling the sun tracker, effectively minimizing the angle of incoming sunlight on the PV panel."

Reviewer#1, Concern #2: Also, in the introduction, some credits to the recent works related to the proposed methods are suggested to enrich the literature in the field of control design. More recent research should be mentioned in references (2022-2024). Some related works can be considered, see for example, Integrated Control Design for Hybrid Grid-Photovoltaic Systems in Distillation Applications: A Reference Model and Fuzzy Logic Approach.

Author response: We thank the reviewer for making this suggestion. We have added for this point at the section "Introduction", paragraph 4, on pages 2-3, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by adding the following explanation:

"Moreover, ANFIS offers the flexibility of fuzzy logic, enabling it to learn from data and automatically adjust parameters [39]. The implementation of ANFIS is less complex compared to other control methods, such as Linear Quadratic Regression (LQR) and Model Predictive Control (MPC). MPC has significantly higher complexity than ANFIS, as it requires solving optimization problems at each time step to determine the optimal control signal [40]. Additionally, LQR has low complexity because it only requires solving a functional quadratic equation. However, LQR is not designed to handle nonlinear systems, such as a triple-axis sun tracker [41]. Meanwhile, the ANFIS approach, which is a hybrid algorithm combining ANN and FIS, can quickly adjust parameters. This makes it highly suitable for real-time systems that demand quick responses and the ability to maintain responsiveness to environmental changes [42], [43]."

We also added some references:

- [39] H. Abouobaida et al., "Integrated Control Design for Hybrid Grid-Photovoltaic Systems in Distillation Applications: A Reference Model and Fuzzy Logic Approach," Sustainability, vol. 16, no. 17, p. 7304, 2024, doi: 10.3390/su16177304.
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- [43] A. Rahman, K. Myo Aung, S. Ihsan, R. M. Raja Ahsan Shah, M. Al Qubeissi, and M. T. Aljarrah, "Solar Energy Dependent Supercapacitor System with ANFIS Controller for Auxiliary Load of Electric Vehicles," Energies, vol. 16, no. 6, p. 2690, Mar. 2023, doi: 10.3390/en16062690.

Reviewer#1, Concern #3: Control techniques inherently suffer from uncertain disturbances. Referencing to Enhanced wind energy conversion system performance using fast smooth second-order sliding mode control with neuro-fuzzy estimation and variable-gain robust exact output differentiator', discuss in detail about possible mitigation strategies. Also, include results on how much the proposed control law could manage to reduce these disturbances?"

Author response: We thank the reviewer for making this suggestion. We have added for this point at the section "Result and Discussion", subsection "Model Performance Analysis", paragraph 5, on page 13, specifically marked with a yellow highlight.

Author action: We have conducted experiment to observe the response system to deal with uncertain disturbances, such as the continuous movement of light and shadows. Therefore, we updated the manuscript by adding the result in Figure 16 with the following explanation:

"Subsequent testing was conducted to analyze the response of the sun tracker system in mitigating uncertain disturbances, such as the continuous movement of light due to cloud movement or shadows from external objects. The testing scenario involved observing the movement of the sun tracker at azimuth and altitude angles of 89° and 72°, respectively. The results of the sun tracker system's response based on ANFIS consequent rules are shown in Figure 16. Based on these tests, the proposed control rules were able to mitigate the effects of disturbances, such as changes in light intensity due to clouds, while maintaining the optimal orientation of the solar panel."

Reviewer#1, Concern #4: The equations in the manuscript are not consistently formatted, lack proper explanation, and are not clearly linked to the corresponding discussion, making them difficult to follow and interpret.

Author response: We thank the reviewer for making this suggestion. We have updated for this point at the section "Proposed Method, subsection "ANFIS Model", paragraph 3 on page 7, and subsection "Mechanical Structure of Sun Tracker", paragraph 2, on page 9, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by adding the following explanation in Equation (5):

"These consequent rules are applied to Eq. (5)."

We also have updated the Equations (20)-(31) to detailed the modified forward kinematic equations with following explanation:

"By applying trigonometric theorems, we obtain,

$J_i x = (a_i \cdot \cos \theta_i + b_i (\cos \theta_i \cdot \cos \alpha_i - \sin \theta_i \cdot \sin \alpha_i)) \cos \beta_i + M_i x$	(20)
$J_i y = (a_i \cdot \cos \theta_i + b_i (\cos \theta_i \cdot \cos \alpha_i - \sin \theta_i \cdot \sin \alpha_i)) \sin \beta_i + M_i y$	(21)

 $J_{i}z = (a_{i}.\sin\theta_{i} + b_{i}(\sin\theta_{i}.\cos\alpha_{i} + \cos\theta_{i}.\sin\alpha_{i})) + M_{i}z$ (22)

In this condition, the arm b_i remains perpendicular at 90° to the base, even when motor M_i moves. This is because point J_i is connected to the triangular plane above it, keeping arm b_i perpendicular. The simulation of this movement is shown in Figure 9. Based on this condition, the angle $\alpha_i = 90 + \theta_i$, so by applying the rules $cos(90 + \theta_1) = -sin \theta_i$ and $sin(90 + \theta_1) = cos \theta_i$, we obtain $sin \alpha_i = cos \theta_i$ and $cos \alpha_i = -sin \theta_i$. Then, by substituting in Eq. (20), Eq. (21), and Eq. (22), the following equations is derived."

For the point *x*,

$J_{i}x = (a_{i} \cdot \cos \theta_{i} + b_{i}(-\cos \theta_{i} \cdot \sin \theta_{i} - \sin \theta_{i} \cdot \cos \theta_{i}) \cos \beta_{i} + M_{i}x$	(23)
$J_i x = (a_i \cdot \cos \theta_i + b_i (-2 \sin \theta_i \cdot \cos \theta_i) \cos \beta_i + M_i x$	(24)
$J_i x = (a_i \cdot \cos \theta_i + b_i \cdot \sin 2\theta_i) \cdot \cos \beta_i + M_i x$	(25)

For the point *y*,

$J_i y = (a_i \cdot \cos \theta_i + b_i (-\cos \theta_i \cdot \sin \theta_i - \sin \theta_i \cdot \cos \theta_i) \sin \beta_i + M_i y$	(26)
$J_i y = (a_i \cdot \cos \theta_i + b_i (-2 \sin \theta_i \cdot \cos \theta_i) \sin \beta_i + M_i y$	(27)
$J_i y = (a_i \cdot \cos \theta_i + b_i \cdot \sin 2\theta_i) \cdot \sin \beta_i + M_i y$	(28)

For the point z,

$$J_{i}z = (a_{i}.\sin\theta_{i} + b_{i}(-\sin\theta_{i}.\sin\theta_{i} + \cos\theta_{i}.\cos\theta_{i}) + M_{i}z$$

$$J_{i}z = (a_{i}.\sin\theta_{i} + b_{i}(1 - 2\sin^{2}\theta_{i}) + M_{i}z$$

$$J_{i}z = a_{i}.\sin\theta_{i} + b_{i}.\cos2\theta_{i} + M_{i}z$$
(29)
(30)
(30)
(31)

We also have updated the manuscript by adding following explanation in Equation (32)-(34):

"The vectors in Eq. (32) can be calculated using the following equations"

"Thus, from Eq. (33) and Eq. (34), the normal vector is expressed as follows"

We also have added the Equations (36)-(38) to detailed the normal vector in Equation (35) with following explanation:

"So that, we obtain,
$v_x = (y_2 - y_1)(z_3 - z_1) - (y_3 - y_1)(z_2 - z_1)$	(36)
$v_y = (x_2 - x_1)(z_3 - z_1) - (x_3 - x_1)(z_2 - z_1)$	(37)
$v_z = (x_2 - x_1)(y_3 - y_1) - (x_3 - x_1)(y_2 - y_1)$	(38)

Based on Eq. (36), Eq. (37), and Eq. (38), the tilt angle of the plane concerning the *x*-axis (θ_x) and the *y*-axis (θ_x) can be determined using the following equations"

Reviewer#1, Concern #5: The presentation of the control technique is unclear and lacks sufficient detail. Key concepts are not explained adequately, and the methodology is not illustrated effectively, making it difficult to understand its implementation and significance.

Author response: We thank the reviewer for making this suggestion. We have added for this point at the Figure 5, on page 7, and updated Figure 6, on page 8, specifically marked with a yellow highlight.

Author action: We have updated the manuscript to detail the proposed control technique methodology by adding the flowchart of ANFIS modeling and solar tracking control system in Figure 5 with the following explanation:

"The flowchart illustrating the entire proposed system, including the ANFIS modeling method and sun tracker control, is shown in Figure 5."

We also have updated "block diagram of proposed tracker system with ANFIS-PCT" in Figure 6 with the following explanation:

"Based on Figure 6, ANFIS 1 model controls the angle (θ) of servo motor 1 based on inputs from P_1 sensor, P_2 sensor, and the initial angle (θ_0) of servo motor 1. ANFIS 2 model controls the angle of servo motor 2 based on inputs from P_2 sensor, P_3 sensor, and the initial angle of servo motor 2. Meanwhile, ANFIS 3 model controls the angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 motor 3. Next, the output angle of each motor is calculated and used to move the three arms of the sun tracker."

Reviewer#1, Concern #6: The comparative analysis is weak. A deeper comparison with other state-of-theart methods, such as Adaptive FIT-SMC Approach for an Anthropomorphic Manipulator with Robust Exact Differentiator and Neural Network-Based Friction Compensation, would give readers a clearer sense of how the proposed method stands in the broader context of robust control research.

Author response: We thank the reviewer for making this suggestion. We have added for this point at the Tables 5-7, on pages 14-15, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by adding the comparison of performance ANFIS consequent rules in Table 5 and Table 6 with the following explanation:

"Further analysis was conducted to determine the system's response to each ANFIS consequent rule in response to changes in light position. The study was performed by comparing the system's response based on Figure 16. This analysis considered characteristics such as rise time, peak time, overshoot, settling time, and steady-state error for both azimuth and altitude movements, which are presented in Table 5 and Table 6. For azimuth movement, second-order showed the most optimal performance, achieving the fastest rise time and settling time with low steady-state error. The second-order response also did not exhibit any overshoot. Meanwhile, the peak time obtained was longer than that of the first-order. In the first-order, the

settling time was unavailable because the system response did not reach a steady-state condition during the observation period. For altitude movement, the analysis also indicated that the second-order performed better than the others. No overshoot occurred in the second-order, as with the azimuth movement. In the first-order, the settling time was also unavailable, as the system response did not reach a steady-state condition. This analysis reveals that second-order is the best choice for controlling both azimuth and altitude movements, making this consequent rule most suitable for implementation in ANFIS-PCT for a triple-axis sun tracker system."

We have also compared of the proposed ANFIS model with other published models in Table 7 with the following explanation:

"Table 7 compares the proposed ANFIS model's performance with several previous models related to sun tracker systems. The comparison aims to validate the performance of the proposed ANFIS model in tracking the sun's position. The models compared include PID-ANN [44], Fast Integral Terminal Sliding Mode Control (FIT-SMC) [68], Neural Network Algorithm with Model Predictive Control (NNA-MPC) [69], PID with Internal Model Controller (PID-IMC) [51], PID with Fuzzy Logic Controller (PID-FLC) [48], PD with Fuzzy Logic Controller (PD-FLC) [46], and Artificial Bee Colony (ABC) [50]. The parameters compared are rise time, settling time, and steady-state error. Based on the comparison, the proposed ANFIS-PCT model demonstrates optimal performance. For the rise time parameter, ANFIS-PCT has a relatively fast time, only behind the FIT-SMC model, which recorded the most rapid rise time of 0.15 seconds. However, compared to other models, ANFIS-PCT is far superior. For the settling time parameter, ANFIS-PCT also shows optimal performance, although it is still behind FIT-SMC, which recorded the fastest time. Meanwhile, for the steady-state error, ANFIS-PCT demonstrates a more stable and accurate system."

We also added some references:

- [68] K. Ali, S. Ullah, A. Mehmood, H. Mostafa, M. Marey, and J. Iqbal, "Adaptive FIT-SMC Approach for an Anthropomorphic Manipulator With Robust Exact Differentiator and Neural Network-Based Friction Compensation," IEEE Access, vol. 10, pp. 3378–3389, 2022, doi: 10.1109/ACCESS.2021.3139041.
- [69] M. Elsisi, K. Mahmoud, M. Lehtonen, and M. M. F. Darwish, "Effective Nonlinear Model Predictive Control Scheme Tuned by Improved NN for Robotic Manipulators," IEEE Access, vol. 9, pp. 64278– 64290, 2021, doi: 10.1109/ACCESS.2021.3075581.

Reviewer#1, Concern #7: The manuscript lacks a detailed discussion on how the various parameters of the proposed controller are selected and tuned. This is highly relevant. So, a more structured approach to tuning these parameters and explaining the trade-offs must be included.

Author response: We thank the reviewer for making this suggestion. We have added for this point at the section "Proposed Method, subsection "ANFIS Model", paragraph 1, on page 6, specifically marked with a yellow highlight.

Author action: We have updated the manuscript to detail the discussion about the parameter selected at the proposed method by adding the following explanation:

"The proposed membership function utilizes a Gaussian function chosen for its flexibility in modeling nonlinear relationships between inputs and outputs [62]. The number of membership functions for each input was determined based on performance evaluation through simulation, where three membership functions per input demonstrated a balance between computational complexity and model accuracy. Using more than three membership functions increases accuracy but significantly adds to computation time, making it unsuitable for real-time sun tracker systems. The learning rate parameter was set to 0.01 after testing, which showed that this value provides stable convergence without compromising training speed. Additionally, the number of training iterations was set to 5000 epochs based on observations indicating that the model achieves minimum error performance within this range."

We also added reference:

[62] V. Radhakrishna, P. V. Kumar, S. A. Aljawarneh, and V. Janaki, "Design and Analysis of a Novel Temporal Dissimilarity Measure using Gaussian Membership Function," in International Conference on Engineering & MIS (ICEMIS), May 2017, pp. 1–5, doi: 10.1109/ICEMIS.2017.8273098.

Reviewer#1, Concern #8: The method's stability is validated using the Lyapunov theory, although this section could benefit from a more thorough discussion. Specifically, the paper could elaborate on the practical implications of the stability guarantees and whether they hold under real-world conditions, particularly under unmodeled dynamics or significant disturbances.

Author response: We express our gratitude for the reviewer's feedback regarding stability validation using Lyapunov theory. We acknowledge that the discussion on system stability has not been explored in depth in this study. We recognize this as a limitation of our research. Therefore, future studies will focus on developing a more comprehensive stability analysis based on Lyapunov theory. Therefore, we have added suggestions for future study at the section "Conclusion", paragraph 3, on page 15, marked with yellow highlights.

Author action: We have updated the manuscript by adding suggestions for future study with the following explanation:

"Further research can be developed by exploring the Lyapunov method to explicitly determine the stability of the sun tracker system, allowing the mathematical proof to support the experimental results that have been conducted."

Reviewer#1, Concern #9: The figures lack clarity, proper labeling, and detailed captions, making interpretation difficult. The result discussion is superficial, lacking depth, critical analysis, and comparison with existing literature.

Author response: We thank the reviewer for this suggestion. We have updated the figures by providing detailed labels in Figure 3 on page 5. We also have tidied up Figures 12 and 17 on pages 5 and 14, respectively, specifically marking them with a yellow highlight. For the result discussion and comparison with existing literature, we have addressed this issue in concern #6 by adding Table 5-7, on pages 14-15.

Author action: We have updated the Figure 4 by adding label on each part and tidied up Figures 12 and 17. The result and comparison with existing literature have been discussed in concern #6.

Reviewer#1, Concern #10: Detail the computer you used to perform the experiments.

Author response: We thank the reviewer for making this suggestion. We have added for this point at the section "Proposed Method", paragraph 1, on page 6, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by adding the following explanation:

"The modeling process of ANFIS and the simulation of the sun tracker system were conducted on a computer with an AMD Ryzen 5 4600H CPU, 16 GB DDR4 RAM, and an NVIDIA GeForce GTX 1650 Ti GPU with 4 GB memory. Additionally, the software used includes Python 3.10 with TensorFlow version 2.12.0."

Reviewer#1, Concern #11: Share an open-access repository to check the results. It will have more impact on your research. You can use GitHub, OceanCode, etc.

Author response: We appreciate the reviewer suggestion to share an open-access repository to verify the research findings. However, we are currently unable to make the repository publicly available because this research is part of a project funded by an institution and is still in the advanced development stage. Therefore, the research code and data are considered intellectual property, and their distribution rights must be protected until all stages of the research are completed. We are committed to sharing the open-access repository once the project is finalized and its intellectual property rights are legally secured.

Author action: -

Reviewer#1, Concern #12: Thoroughly proofread the paper for typos and linguistic improvements.

Author response: Thank you for the suggestion to thoroughly proofread the paper. We acknowledge the importance of ensuring that the manuscript is free from typographical errors and linguistic inconsistencies to maintain clarity and professionalism.

Author action: We have updated by proofreading in the entire manuscript.

Reviewer#1, Concern #13: Make sure that all abbreviations are elaborated/defined.

Author response: We thank the reviewer for making this suggestion. We have added for this point at the Table 2, on page 4, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by adding Table 2 with the following explanation:

"For convenience, the abbreviations used in this paper are summarized in Table 2."

Reviewer#1, Concern #14: Figures are needed to regenerate.

Author response: Thank you for pointing out the need to regenerate the figures. We have regenerated Figures 3, 6, 12, and 17, on pages 5, 8, 11, 14, respectively, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by regenerating Figures 3, 6, 12, and 17.

Reviewer#2, Concern #1: Could the authors explain why ANFIS was chosen for this application over other advanced control approaches like Model Predictive Control or Linear Quadratic Regression?

Author response: We thank the reviewer for making this suggestion. We have added for this point at the section "Introduction", paragraph 4, on pages 2-3, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by adding the reasons why ANFIS was chosen with the following explanation:

"The implementation of ANFIS is less complex compared to other control methods, such as Linear Quadratic Regression (LQR) and Model Predictive Control (MPC). MPC has significantly higher complexity than ANFIS, as it requires solving optimization problems at each time step to determine the optimal control signal [40]. Additionally, LQR has low complexity because it only requires solving a functional quadratic equation. However, LQR is not designed to handle nonlinear systems, such as a triple-axis sun tracker [41]. Meanwhile, the ANFIS approach, which is a hybrid algorithm combining ANN and FIS, can quickly adjust parameters. This makes it highly suitable for real-time systems that demand quick responses and the ability to maintain responsiveness to environmental changes [42], [43]."

We also added some references:

- [40] M. Schwenzer, M. Ay, T. Bergs, and D. Abel, "Review on Model Predictive Control: An Engineering Perspective," Int. J. Adv. Manuf. Technol., vol. 117, no. 5–6, pp. 1327–1349, Nov. 2021, doi: 10.1007/s00170-021-07682-3.
- [41] H. Matsui, "Quadratic Regression for Functional Response Models," Econom. Stat., vol. 13, pp. 125– 136, Jan. 2020, doi: 10.1016/j.ecosta.2018.12.003.
- [42] A. Habibi, B. Yousefi, A. N. Shirazi, and M. Rezvani, "Adaptive Neuro-Fuzzy Damping Controller of Grid-Connected Microgrid Hybrid System Integrating Wind Farms and Batteries," IEEE Access, vol. 12, pp. 8022–8037, 2024, doi: 10.1109/ACCESS.2023.3312272.
- [43] A. Rahman, K. Myo Aung, S. Ihsan, R. M. Raja Ahsan Shah, M. Al Qubeissi, and M. T. Aljarrah, "Solar Energy Dependent Supercapacitor System with ANFIS Controller for Auxiliary Load of Electric Vehicles," Energies, vol. 16, no. 6, p. 2690, Mar. 2023, doi: 10.3390/en16062690.

Reviewer#2, Concern #2: Table 4 compares PID and ANN controllers; could alternative controllers, such as hybrid MPC-ANN systems, provide further insights?

Author response: We thank the reviewer for making this suggestion. We have added for this point at the section "Result and Discussion", subsection "System Performance Comparison", paragraph 1, on pages 14-15, specifically marked with a yellow highlight.

Author action: We compared the proposed ANFIS model with other published models in Table 7 to compare with NNA-MPC and other systems, such as FIT-SMC, PID-IC, PID-FLC, PD-FLC, and ABC. We updated the manuscript by adding the following explanation:

"Table 7 compares the proposed ANFIS model's performance with several previous models related to sun tracker systems. The comparison aims to validate the performance of the proposed ANFIS model in tracking the sun's position. The models compared include PID-ANN [44], Fast Integral Terminal Sliding Mode Control (FIT-SMC) [68], Neural Network Algorithm with Model Predictive Control (NNA-MPC) [69], PID with Internal Model Controller (PID-IMC) [51], PID with Fuzzy Logic Controller (PID-FLC) [48], PD with Fuzzy Logic Controller (PD-FLC) [46], and Artificial Bee Colony (ABC) [50]. The parameters compared are rise time, settling time, and steady-state error. Based on the comparison, the proposed ANFIS-PCT model demonstrates optimal

performance. For the rise time parameter, ANFIS-PCT has a relatively fast time, only behind the FIT-SMC model, which recorded the most rapid rise time of 0.15 seconds. However, compared to other models, ANFIS-PCT is far superior."

We also added some references:

- [68] K. Ali, S. Ullah, A. Mehmood, H. Mostafa, M. Marey, and J. Iqbal, "Adaptive FIT-SMC Approach for an Anthropomorphic Manipulator With Robust Exact Differentiator and Neural Network-Based Friction Compensation," IEEE Access, vol. 10, pp. 3378–3389, 2022, doi: 10.1109/ACCESS.2021.3139041.
- [69] M. Elsisi, K. Mahmoud, M. Lehtonen, and M. M. F. Darwish, "Effective Nonlinear Model Predictive Control Scheme Tuned by Improved NN for Robotic Manipulators," IEEE Access, vol. 9, pp. 64278– 64290, 2021, doi: 10.1109/ACCESS.2021.3075581.

Reviewer#2, Concern #3: How does the computational complexity of the proposed ANFIS parallelisation control compare to the other methods presented, particularly for real-time applications?

Author response: We thank the reviewer for making this suggestion. We have addressed this issue to explain the comparison of the computational complexity of the proposed ANFIS with other methods, such as MPC and LQR, that have been discussed in concern #1.

Author action: We have updated the manuscript by adding following explanation:

"The implementation of ANFIS is less complex compared to other control methods, such as Linear Quadratic Regression (LQR) and Model Predictive Control (MPC). MPC has significantly higher complexity than ANFIS, as it requires solving optimization problems at each time step to determine the optimal control signal [40]. Additionally, LQR has low complexity because it only requires solving a functional quadratic equation. However, LQR is not designed to handle nonlinear systems, such as a triple-axis sun tracker [41]. Meanwhile, the ANFIS approach, which is a hybrid algorithm combining ANN and FIS, can quickly adjust parameters. This makes it highly suitable for real-time systems that demand quick responses and the ability to maintain responsiveness to environmental changes [42], [43]."

We also have added the advantage of ANFIS parallelization control complexity proportional to the response system produced:

"ANFIS-PCT offers an optimal balance between computational complexity, robustness against nonlinearity, and real-time responsiveness, making it the best solution for triple-axis sun tracker systems"

Reviewer#2, Concern #4: The text identifies energy consumption as a disadvantage of the triple-axis device. Have the authors researched and tested energy-efficient strategies to address this issue?

Author response: We thank the reviewer for making this suggestion. Energy-efficient strategies are not yet part of our research scope. We acknowledge that this limitation of the study needs to be further studied. Future research will focus on exploring energy-saving strategies. Therefore, we have added suggestions for future research at the section "Conclusion", on page 15, paragraph 3, specifically marked with a yellow highlight.

Author action: We updated the manuscript by adding the following suggestion:

"Additionally, future research will focus on exploring energy-saving strategies, including optimizing by reducing unnecessary servo motor movements, as well as evaluating the comparison between the energy produced and the total energy consumed."

Reviewer#2, Concern #5: The second-order consequent rule is identified as optimal. What specific factors contribute to its superior performance compared to the first- and third-order rules in this context?

Author response: We thank the reviewer for making this suggestion. We have added for this point at the section "Results and Discussion", subsection "Model Performance Analysis", paragraph 6, on page 14, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by adding the reasons why the second-order was chosen in the following explanation:

"Further analysis was conducted to determine the system's response to each ANFIS consequent rule in response to changes in light position. The study was performed by comparing the system's response based on Figure 16. This analysis considered characteristics such as rise time, peak time, overshoot, settling time, and steady-state error for both azimuth and altitude movements, which are presented in Table 5 and Table 6. For azimuth movement, second-order showed the most optimal performance, achieving the fastest rise time and settling time with low steady-state error. The second-order response also did not exhibit any overshoot. Meanwhile, the peak time obtained was longer than that of the first-order. In the first-order, the settling time was unavailable because the system response did not reach a steady-state condition during the observation period. For altitude movement, the analysis also indicated that the second-order performed better than the others. No overshoot occurred in the second-order, as with the azimuth movement. In the first-order, the settling time was also unavailable, as the system response did not reach a steady-state condition. This analysis reveals that second-order is the best choice for controlling both azimuth and altitude movements, making this consequent rule most suitable for implementation in ANFIS-PCT for a triple-axis sun tracker system."

We also added the results comparison in Figure 16 with data analysis in Tables 5-6.

Reviewer#2, Concern #6: How would the performance of the proposed system vary under partially shaded conditions, and is ANFIS robust enough to handle such scenarios compared to other controllers?

Author response: We thank the reviewer for making this suggestion. We have added for this point about partial shading condition at the section "Result and Discussion", subsection "Model Performance Analysis", paragraph 5, on page 13 and the result of ANFIS in subsection "System Performance Comparison", paragraph 1, on pages 14-15, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by adding discussion about partial shading condition with the following explanation:

"Under partial shading conditions, where some sensors or PV panels receive reduced light intensity due to shadows from clouds or surrounding objects, the tracking system may face challenges in maintaining the optimal orientation of the solar panel toward the sun."

We also have added the result that the proposed ANFIS-PCT method is more stable than other controllers with the following explanation:

"For the rise time parameter, ANFIS-PCT has a relatively fast time, only behind the FIT-SMC model, which recorded the most rapid rise time of 0.15 seconds. However, compared to other models, ANFIS-PCT is far superior. For the settling time parameter, ANFIS-PCT also shows optimal performance, although it is still behind FIT-SMC, which recorded the fastest time. Meanwhile, for the steady-state error, ANFIS-PCT demonstrates a more stable and accurate system."

Reviewer#2, Concern #7: The authors focus on minimizing the solar incidence angle; could they elaborate on the practical implications of this in terms of energy efficiency and compare it with systems that prioritize other optimization metrics?

Author response: We thank the reviewer for making this suggestion. We have added for this point at the section "Introduction", paragraphs 4-5, on pages 2-3, specifically marked with a yellow highlight.

Author action: We have updated the manuscript by adding the practical implications in terms of energy output with the following explanation:

"This research focuses on minimizing the solar incidence angle to enhance the electrical energy production of PV systems. When the solar incidence angle on the panel surface approaches zero, the amount of sunlight absorbed by the PV reaches its maximum, directly increasing the generated electrical output."

Meanwhile, for comparison with other system, we have discussed this issue in concern #1

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ANFIS Parallelization Control on Triple-Axis Sun Tracker to Minimize Solar Rays Incidence Angle on Photovoltaic

Hari Anna Lastya, Yuwaldi Away, Tarmizi, Ira Devi Sara, Roslidar, Andri Novandri

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RESEARCH ARTICLE

ANFIS Parallelization Control on Triple-Axis Sun Tracker to Minimize Solar Rays Incidence Angle on Photovoltaic

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ABSTRACT This study proposes an Adaptive Neuro-Fuzzy Inference System (ANFIS) based on model with Parallelization Control Technique (PCT) implemented in a triple-axis sun tracker system. The system aims to maximize solar energy absorption by minimizing the angle of incidence of sunlight on Photovoltaic (PV) panels. It is designed with three manipulator arms, each controlled in parallel by a distinct ANFIS model. The primary goal is to adjust the PV panel orientation to optimal azimuth and altitude angles. The tetrahedron sensor is employed to detect the direction of sunlight. This study tests various types of consequent rules to find the optimal configuration for each ANFIS model, including first-order, second-order, and third-order polynomial functions. The analysis results show that the second-order consequent rule provides the highest accuracy across the three ANFIS models. The proposed system can cover azimuth range from 0° to 360° and altitude angle from 60° to 90°. The experiment also demonstrated that the system consistently moves toward a stable condition, even in the presence of minor disturbances. These findings indicate that ANFIS with PCT can minimize the angle of sunlight incidence, enhance system flexibility, and accelerate response time, making it a viable solution for increasing energy harvesting by PV panels.

INDEX TERMS ANFIS, parallelization control, photovoltaic, sun tracker, triple-axis.

I. INTRODUCTION

The sun tracker system is designed to automatically follow the sun's movement, maximizing sunlight reception on Photovoltaic (PV) panels [1]. This technology is essential in increasing energy production in PV systems, especially in areas with high sunlight intensity. PV efficiency heavily depends on the angle of sunlight incidence on the PV surface. The more optimal the angle, the greater the amount of sunlight absorbed, increasing the electrical energy produced [2], [3]. To maximize generated energy, the orientation

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of the panels needs to be adjusted in real-time so that the PV always maintains an optimal angle to the sunlight [4], [5], [6]. Conventional solar power plants are generally installed statically, so PV panels do not receive optimal sunlight exposure, especially in the morning and evening [7],. A sun tracker system can dynamically adjusted the PV orientation to remain perpendicular to the sunlight, thereby maximizing the electrical energy obtained [9], [10], [11]. Sun tracker systems have been discussed in several studies, including in [12], where a comparison between fixed PV systems and sun trackers was conducted. The results showed that sun trackers can increase electricity generation by 30% compared to fixed PV systems. Another study in [13] examined a sun tracker system

using a Stewart platform mechanism, demonstrating that the sun tracker system can enhance energy generation by 32% compared to fixed PV systems. Additionally, [14] compares energy produced and consumed by sun tracker systems. The findings indicate that the total energy obtained from a sun tracker system is 26.9% higher than from a fixed PV system, with the energy consumption of the sun tracker reaching 5.63% or around 21.22 Wh and total energy production of 376.85 Wh. These studies show that sun trackers are superior to fixed PV systems. Furthermore, as discussed in [15], the popularity of sun tracker systems continues to rise along with the growing use of solar energy as an alternative energy source. Further developments in sun tracker systems cover various aspects, including manual control through internet networks as studied in [16] and [17], bluetooth-based control as examined in [18], and automatic control using solar trajectory models as explored in [19] and [20].

In its implementation, a sun tracker requires an effective sensor to accurately detect the sun's position coordinates. This study proposes a type of sensor called a tetrahedron sensor. The survey of the tetrahedron sensor was first introduced in [21], which analyzed the design and structure of the sensor, consisting of three photoresistors. The study's results demonstrated that the tetrahedron sensor could detect the sun's position with a maximum wide Field of View (FOV) of 289.4° and an accuracy of $\pm 1.67^{\circ}$. Further research on the tetrahedron sensor is discussed in [22], which focuses on developing a sensor based on phototransistors to replace photoresistors. Additionally, [23] examined the effect of the tetrahedron sensor's dimensions on the sun tracker's performance in tracking the sun's position. The results showed that increasing the height of the tetrahedron correlates with an increase in FOV, where a tetrahedron with a height of 4.5 cm has an FOV of 289.4°, while a height of 10.2 cm reaches an FOV of 310°.

An appropriate control algorithm and drive mechanism are needed to control the orientation movement of a sun tracker. The control algorithm is necessary to quickly and stably adjust the panel position, reducing energy losses caused by suboptimal angles of incidence. Meanwhile, the drive mechanism is required to support smooth and precise movements. Several studies have examined single-axis and dual-axis drive mechanisms with various algorithms, as shown in Table 1. Based on these studies, the design of the control mechanism in a sun tracker significantly influences the system's response time in following the sun's movement. On the other hand, some studies have developed triple-axis drive mechanisms. This mechanism is designed to improve the vertical orientation adjustment of PV panels. In [24], it is stated that the efficiency of commercial PV typically ranges from 10-20%. Applying a triple-axis mechanism to the sun tracker increases PV efficiency by up to 25%. In [25], it is revealed that the power output generated by PV on a triple-axis sun tracker is 19% greater than that of a dual-axis mechanism. This improvement is due to the triple-axis mechanism's ability to

adjust the PV panel's height, enabling it to prevent shadows from surrounding objects from falling onto the panel surface. Furthermore, [26] states that a triple-axis sun tracker can be implemented on a mobile platform, allowing the panel to adjust its orientation to maintain an optimal position even if the platform moves. Although triple-axis sun trackers have significant potential for improving PV efficiency, there are still technical challenges in determining a control method to optimize panel orientation. With the proper control method, the system can adapt to changes in the sun's position and avoid shadows from objects falling on the panel surface [27]. One approach capable of adapting to changing conditions is the Adaptive Neuro-Fuzzy Inference System (ANFIS).

ANFIS is an algorithm that combines approaches from Artificial Neural Networks (ANN) and Fuzzy Inference Systems (FIS) to model complex relationships between inputs and outputs [28]. FIS handles uncertain data using fuzzy rules and membership functions to map input values into fuzzy sets [29]. Meanwhile, ANN is responsible for the learning process, where parameters within the fuzzy system, such as membership functions and fuzzy rules, are automatically optimized based on the provided training data [30]. The main processes in ANFIS include fuzzification, which transforms input values into fuzzy values; fuzzy inference, which generates fuzzy output based on fuzzy rules; and defuzzification, which converts the fuzzy output into a numerical value [31], [32]. Several studies have explored the application of ANFIS in various fields. For example, in [33], ANFIS was applied to model machine behaviour in a gas turbine by estimating its operational parameters and improving its performance and durability. Furthermore, [34] discusses the application of ANFIS for controlling dynamic force and position in a Programmable Universal Machine for Assembly (PUMA) robot. Another study [35], applied ANFIS to model the behaviour of an air spring system, which was used to control the solenoid valve of the air spring system to reduce mass acceleration. In addition, other studies have discussed the application of ANFIS in controlling sun trackers. For instance, [36] compared the performance of a Proportional Integral Derivative (PID) controller with ANFIS, with both algorithms optimized using the Firefly Algorithm (FA) to enhance system speed and stability. The findings showed that the ANFIS-FA combination significantly reduced overshoot and accelerated settling time. Furthermore, [37] explored the ANFIS application by comparing single-axis and dual-axis sun tracker mechanisms, concluding that ANFIS with five membership functions was more optimal in controlling both sun tracker mechanisms, yielding high prediction accuracy and low error. Additionally, [38] conducted further analysis on ANFIS as a sun tracker controller, examining the effect of the number of membership functions on model training. This study revealed that the number of membership functions directly affects model performance, with an increase in membership functions leading to reduced error. Moreover, ANFIS offers the flexibility of fuzzy logic, enabling it to

Paper	Year	Algorithm	Control Mechanism	Rise Time (s)	%Error
Yuwaldi Away et al. [44]	2023	PID-ANN	Dual-Axis	2.18	1.75%
Andri Novandri et al. [45]	2022	PID	Dual-Axis	1.85	2.6%
Fitri Rahmah et al. [46]	2022	Fuzzy-PD	Single-Axis	7.43	0.43%
Baisrum et al. [47]	2021	ANFIS	Single-Axis	-	1.25%
Imam Abadi et al. [48]	2020	Fuzzy-PID	Dual-Axis	8.2	-
Jalal Farazi et al. [49]	2020	PO-ANN	Dual-Axis	0.94	-
Zubairu A. Yusuf et al. [50]	2019	ABC	Single-Axis	2.37	-
Bamigboye O. Oladayo et al. [51]	2016	IMC-PID	Dual-Axis	1.78	-
Mirza Muhammad Sabir et al. [52]	2016	PID	Dual-Axis	2.2	0.5%

TABLE 1. Literature review of control mechanism on sun tracker.

learn from data and automatically adjust parameters [39]. The implementation of ANFIS is less complex compared to other control methods, such as Linear Quadratic Regression (LQR) and Model Predictive Control (MPC). MPC has significantly higher complexity than ANFIS, as it requires solving optimization problems at each time step to determine the optimal control signal [40]. Additionally, LQR has low complexity because it only requires solving a functional quadratic equation. However, LQR is not designed to handle nonlinear systems, such as a triple-axis sun tracker [41]. Meanwhile, the ANFIS approach, which is a hybrid algorithm combining ANN and FIS, can quickly adjust parameters. This makes it highly suitable for real-time systems that demand quick responses and the ability to maintain responsiveness to environmental changes [42], [43]. Based on these studies, it is concluded that the ANFIS model can improve control performance in sun tracker systems, especially with additional optimization or increased membership functions. This makes ANFIS a practical approach for controlling PV panel orientation.

Based on these studies, most current sun tracker systems still rely on single-axis or dual-axis mechanisms, which have limitations in vertical adjustments and in avoiding shadows from objects surrounding the panels. On the other hand, research on triple-axis mechanisms is still minimal. Additionally, optimization techniques are needed to enhance the performance of the ANFIS algorithm in managing the complexity of sun tracker systems, particularly in triple-axis mechanisms. As a solution, the sun tracker system with a triple-axis drive mechanism is proposed. This proposed mechanism uses three manipulator arms, each driven by a servo motor. These three arms adjust the PV panel orientation along three axes, allowing the sun tracker to control movement at azimuth and altitude angles. A tetrahedron sensor consisting of three phototransistors arranged on each side of the tetrahedron, detects the sun's position. Additional optimization of the ANFIS algorithm is proposed to control the servo motors by applying the Parallelization Control Technique (PCT). This control method aims to divide computational processes into parts that can be executed in parallel, thereby enhancing computational efficiency and processing speed, especially in complex tasks. PCT enables multiple control processes to run simultaneously, reducing latency and improving system responsiveness. ANFIS-PCT offers an optimal balance between computational complexity, robustness against nonlinearity, and real-time responsiveness, making it the best solution for triple-axis sun tracker systems. In this proposed sun tracker, the system is divided into three processes that are responsible for controlling each servo motor's rotation angle. Input data is obtained from the tetrahedron sensor readings, with input variables varying for each process, resulting in distinct ANFIS models. ANFIS modelling is conducted by designing the network structure, determining the membership functions, and establishing fuzzy rules. Within the fuzzy rules is a consequent rule, part of the fuzzy rule that defines the output based on the fulfilled input conditions. An analysis of the consequent rules is necessary to achieve an optimal model. This study examines three types of consequent rules to identify the most optimal model. The three types of proposed consequent rules are polynomial functions of first-order, second-order, and third-order. Each of these orders has different complexity and mapping capabilities in identifying the relationship between inputs and outputs, requiring evaluation to determine the most suitable model for the sun tracker. This research focuses on minimizing the solar incidence angle to enhance the electrical energy production of PV systems. When the solar incidence angle on the panel surface approaches zero, the amount of sunlight absorbed by the PV reaches its maximum, directly increasing the generated electrical output.

The novelty of this research lies in the implementation of PCT in ANFIS, which enables the division of computational processes into multiple parts running concurrently. Additionally, this study analyzes various consequent rule configurations in the ANFIS model, including first-order, second-order, and third-order polynomial functions, to determine the most optimal configuration. The main contributions of this paper are as follows:

• We propose a sun tracker system using a triple-axis mechanism consisting of three manipulator arms to control the azimuth and altitude angles. This system enables PV panels to adjust their angles optimally to the direction of incoming sunlight.

- We propose an ANFIS algorithm with PCT to control the movement of the sun tracker through separate control processes, making the system more responsive and accurate.
- We demonstrate that the second-order consequent rule provides the best performance in controlling the sun tracker, effectively minimizing the angle of incoming sunlight on the PV panel.

For convenience, the abbreviations used in this paper are summarized in Table 2.

Abbreviation	Meaning
ANFIS	Adaptive Neuro-Fuzzy Inference System
ANN	Artificial Neural Networks
CV	Coefficient of Variation
FIS	Fuzzy Inference Systems
LSE	Least Squares Estimation
MAE	Mean Absolute Error
MAPE	Mean Absolute Percentage Error
PCT	Parallelization Control Technique
PID	Proportional Integral Derivative
PV	Photovoltaic
RMSE	Root Mean Squared Error

TABLE 2. Summary of abbreviations.

II. MATERIAL AND METHODS

A. TETRAHEDRON SENSOR

The tetrahedron sensor is a type of sensor used to detect the position of sunlight. This sensor has a pyramid shape with three sides, each equipped with a light sensor in the form of a phototransistor. Figure 1 shows a phototransistor in the center of each side of the pyramid, with each position labelled P_1 , P_2 , and P_3 . The sensor has a height of 10 cm and a base length of 5 cm. The type of light sensor and the dimensions of the tetrahedron are based on previous studies [22], [23]. The tetrahedron sensor operates on the principle of comparing values from each phototransistor. Based on these comparisons, the sensor can determine the sun's position regarding azimuth and altitude.

B. ADAPTIVE NEURO-FUZZY INFERENCE SYSTEM

ANFIS is a hybrid intelligent system that combines the strengths of fuzzy logic and ANN. Fuzzy logic provides a reasoning approach that mimics human thinking and can handle uncertainty and ambiguity. At the same time, ANN can learn from data and recognize complex patterns [53], [54]. The ANFIS architecture consists of several layers, each responsible for specific operations. The first layer performs fuzzification, where membership functions map input values to fuzzy sets. The second layer is the rule layer, where the firing strength of fuzzy rules is calculated. The third layer



FIGURE 1. Tetrahedron sensor.

normalizes the firing strengths, while the fourth layer generates the output by multiplying the normalized firing strength with the consequent part of the fuzzy rules. Finally, the output layer combines these results to produce the final output [55].

ANFIS is trained to optimize fuzzy parameters through a learning method that combines the concepts of ANN and fuzzy. The training starts by determining the initial structure of ANFIS, including fuzzy rules, membership functions, and rule types [56]. Training data guides the training process, where the system updates the membership function and consequent parameters [57]. The training process typically consists of two phases: forward pass and backward pass. In the first process, the forward pass, input is fed into ANFIS, and the output is computed through the fuzzy inference mechanism, including fuzzification, firing strength calculation, normalization, and defuzzification to produce the final output [58]. The proposed ANFIS network structure in this study is shown in Figure 2. The first layer is the fuzzification layer, where each node in this layer calculates the membership degree of each input based on the corresponding membership function. The membership function of each input can be calculated using the following equation [59],

$$\mu_i(x_i) = f_i(x_i) \tag{1}$$

where, $\mu_j(x_i)$ is the membership degree for input x_i in the fuzzy set *j* and $f_j(x_i)$ is the membership function of input x_i in the fuzzy set *j*. In this study, a Gaussian Membership Function is used, which is expressed in the following equation,

$$f(x) = gaussian(x; c, \sigma) = e^{-\frac{1}{2}\left(\frac{x-c}{\sigma}\right)^2}$$
(2)

where, c is the mean value that serves as the center of the membership function, and σ is the standard deviation that determines the width of the membership function.

The second layer is the rule layer, where each node represents the firing strength for each fuzzy rule formed based on the combination of membership functions for each input. The firing strength is calculated as the product of the input signals that represent the premises in the fuzzy rules, as expressed in



FIGURE 2. The architecture of ANFIS network.

the following equation,

$$w_i = \prod_{i=1}^{3} \mu_j(x_i)$$
 (3)

where, w_i represents the output firing strength for rule *i*. Then, the firing strength values are normalized in the third layer, the normalization layer. This process ensures that the relative contribution of each fuzzy rule is correctly accounted for so that the total firing strength of all rules equals 1. The normalization process is performed using the following equation,

$$\overline{w_i} = \frac{w_i}{\sum_{i=1}^N w_i} \tag{4}$$

where, $\overline{w_i}$ represents the normalized firing strength and N is the number of fuzzy rules. Next, in the fourth layer, the defuzzification layer, each node multiplies the normalized firing strength by the output of the consequent fuzzy rule using the following equation,

$$z_i = \overline{w_i} \cdot f(x_i) \tag{5}$$

where, z_i represents the defuzzified output for input x_i and $f(x_i)$ represents the output of the consequent rule for rule *i*. The consequent rule is a mathematical expression that determines the fuzzy output based on the input and the existing rules.

Next, in the fifth layer is the output layer. In this layer, each node combines all the signals received from the previous layers to produce the final output of the ANFIS, as expressed by the following equation,

$$y = \sum_{i=1}^{N} z_i \tag{6}$$

The consequent parameters are updated using the Least Squares Estimation (LSE) method by calculating the error between the system output y and the target output y_t , based

on the total dataset *m*. The error is defined as follows,

$$E = \frac{1}{2} \sum_{i=1}^{m} (y_i - y_{t,i})^2$$
(7)

After that, in the second process, the backward pass is performed using the backpropagation method to minimize the error by updating the parameters c and σ of the membership function based on the calculated error. To update the parameter c, the following equation is used,

$$c_{new} = c_{old} - \eta \frac{\partial E}{\partial c} \tag{8}$$

where, $\frac{\partial E}{\partial c}$ is the partial derivative of the error concerning c and η is the learning rate. Then, to update the parameter σ , the following equation is used,

$$\sigma_{new} = \sigma_{old} - \eta \frac{\partial E}{\partial \sigma} \tag{9}$$

where, $\frac{\partial E}{\partial \sigma}$ is the partial derivative of the error concerning σ . This process is repeated until the error reaches a minimum value or until a certain number of iterations is reached.

C. SUN TRACKER SYSTEM

Figure 3 shows the physical device of the sun tracker system. The proposed design implements a triple-axis mechanism with three manipulator arms. This mechanism allows the system to follow the sun's position more quickly as the motors move in parallel. The system uses servo motors as its actuators.



FIGURE 3. Proposed triple-axis sun tracker.



FIGURE 4. The movement of sun's position.

In the testing process, the sun tracker system is compared with the sun's movement path to evaluate the performance of the proposed system. Figure 4 illustrates the position of the sun relative to the tracker. Two main parameters are used to determine the sun's position: azimuth and altitude. Azimuth is the horizontal angle measured clockwise from the north. An angle of 90° means the sun is in the east, 180° in the south, and 270° in the west. Azimuth indicates the sun's direction along the horizon [60]. Meanwhile, altitude measures the sun's height above the horizon, calculated from the horizontal line to the sun's position. This angle changes throughout the day, starting at 0° when the sun rises, reaching its peak at noon, and then returning to 0° when the sun sets [61]. The sun's movement path can be calculated using astronomical formulas based on location and time. The equation to calculate the solar azimuth angle (ϕ_S) is expressed as follows,

$$\sin \phi_S = \frac{\cos \delta \cdot \sin \gamma_H}{\cos \varphi_S} \tag{10}$$

where, δ is the solar declination angle, which can be calculated using the following equation,

$$\delta = 23.45^{\circ} \, . \, \sin\left(360 \, . \, \frac{284 + n}{365}\right) \tag{11}$$

where, *n* is the day number in the year. Meanwhile, γ_H is the solar hour angle, expressed as follows,

$$\gamma_H = 15^{\circ} \ (T_r - 12) \tag{12}$$

where, T_r is the true time, ranging from 0 to 24 hours. Then, φ_S is the solar altitude angle, expressed as follows,

$$\sin \varphi_S = \sin \omega \, . \, \sin \delta + \cos \omega \, . \, \cos \delta \, . \, \cos \gamma_H \qquad (13)$$

where, ω represents the latitude coordinate based on the location on earth.

III. PROPOSED METHOD

The proposed method includes ANFIS modelling and determining the most optimal consequent rule to be applied. It also explains the proposed mechanical structure in the sun tracker system, which aims to optimize the movement of the solar panels to enhance solar energy absorption efficiency. The modeling process of ANFIS and the simulation of the sun tracker system were conducted on a computer with an AMD Ryzen 5 4600H CPU, 16 GB DDR4 RAM, and an NVIDIA GeForce GTX 1650 Ti GPU with 4 GB memory. Additionally, the software used includes Python 3.10 with TensorFlow version 2.12.0. The flowchart illustrating the entire proposed system, including the ANFIS modeling method and sun tracker control, is shown in Figure 5.

A. ANFIS MODEL

In this study, ANFIS is used to control the movement of servo motors based on the light intensity readings from the tetrahedron sensor. The rotation of the motors affects the movement of the manipulator arms, which direct the PV towards the sun. This study proposes ANFIS-PCT, consisting of three ANFIS models, each responsible for controlling a different motor, as shown in Figure 6, with the structure of each network shown in Table 3. The proposed membership function utilizes a Gaussian function chosen for its flexibility in modeling nonlinear relationships between inputs and outputs [62]. The number of membership functions for each input was determined based on performance evaluation through simulation, where three membership functions per input demonstrated a balance between computational complexity and model accuracy. Using more than three membership functions increases accuracy but significantly adds to computation time, making it unsuitable for real-time sun tracker systems. The learning rate parameter was set to 0.01 after testing, which showed that this value provides stable convergence without compromising training speed. Additionally, the number of training iterations was set to 5000 epochs based on observations indicating that the model achieves minimum error performance within this range.

TABLE 3. Proposed ANFIS structure.

Parameter	Value	Description
Number of input	3	Number of nodes in the input layer
Number of output	1	Number of nodes in the output layer
Number of fuzzy MF 1	3	Number of membership functions at input node 1
Number of fuzzy MF 2	3	Number of membership functions at input node 2
Number of fuzzy MF 3	3	Number of membership functions at input node 3
Membership function	Gaussian function	Membership function at input
Number of rules	27	Number of rules fuzzy
Number of datasets	1945	Number of data for training process
Learning rate	0.01	ANFIS learning rate parameter

Based on Figure 6, ANFIS 1 model controls the angle (θ) of servo motor 1 based on inputs from P_1 sensor, P_2 sensor, and the initial angle (θ_0) of servo motor 1. ANFIS 2 model controls the angle of servo motor 2 based on inputs from P_2 sensor, P_3 sensor, and the initial angle of servo motor 2. Meanwhile, ANFIS 3 model controls the angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor, P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor , P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor , P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor , P_1 sensor , and the initial angle of servo motor 3 based on inputs from P_3 sensor , P_1 sensor , and the initial angle of servo motor 3 based to move the three arms of the sun tracker.

There is a consequent rule in defuzzification, obtaining results based on fuzzy rules by describing the mathematical relationship between input and output [63]. The parameters in the consequent rule are optimized during the training process to ensure that the model can accurately predict the output based on the given data. This paper proposes three types of consequent rules: polynomial functions of first-order, secondorder, and third-order. These consequent rules are applied to



FIGURE 5. Flowchart of ANFIS modeling and solar tracking control system.

Eq. (5). The first-order function is expressed as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + r$$
(14)

where, $f(x_i)$ represents the output of the consequent rule, p_i is the first-order parameter for input x_i , and r is the bias constant of the rule. Meanwhile, for the second-order function, the equation is as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + \sum_{i=1}^{3} q_i x_i^2 + \sum_{1 \le i < k \le 3} c_{i,k} x_i x_k + r \quad (15)$$

where, q_i is the second-order parameter for input x_i and $c_{i,k}$ is the parameter for the cross terms between inputs x_i and x_k .

Then, for the third-order function, the equation is as follows,

$$f(x_i) = \sum_{i=1}^{3} p_i x_i + \sum_{i=1}^{3} q_i x_i^2 + \sum_{1 \leq i < k \leq 3} c_{i,k} x_i x_k + \sum_{i=1}^{3} t_i x_i^3 + r \quad (16)$$

where, t_i is the second-order parameter for input x_i .

B. MECHANICAL STRUCTURE OF SUN TRACKER

This sun tracker system configuration uses three manipulator arms, as shown in Figure 7. The model of the manipulator arms is arranged in a parallel configuration, with servo motors as the actuators. These three arms are connected to a triangular plane that serves as the base for the PV. Points J_1 , J_2 , and J_3 connect the plane to the manipulator arms. The height of



FIGURE 6. Block diagram of proposed tracker system with ANFIS-PCT.

these points will affect the orientation of the PV in following the sun's movement.



FIGURE 7. Triple-arm manipulator configuration on sun tracker system.

The configuration of the manipulator arm is shown in Figure 8(a). The arm consists of the upper arm (b_i) and the lower arm (a_i) , with lengths of 3.7 cm and 1.6 cm, respectively. Additionally, there are two connection points: the elbow point (E_i) and the end-effector point (J_i) , as well as a drive point M_i as the motor (for i = 1, 2, 3). The E_i point is the connection between the lower and upper arm, while J_i is the connection between the upper arm and the



FIGURE 8. The configuration of arm manipulator: (a) arm structure design, (b) system mechanism.

base plane where the PV is mounted. Figure 8(b) shows the drive mechanism of the manipulator arm. The angle β_i is the orientation angle of the manipulator arm relative to the *x*-axis. The movement of motor M_i will create an angle θ_i . This angle will affect the value of angle α_i at point E_i , causing the coordinates at point J_i to change. These coordinate changes can be calculated using the following forward kinematic equation [64], [65],

$$J_i x = (a_i \cdot \cos \theta_i + b_i \cdot \cos (\theta_i + \alpha_i)) \cos \beta_i + M_i x \quad (17)$$

$$J_i y = (a_i \cdot \cos \theta_i + b_i \cdot \cos (\theta_i + \alpha_i)) \sin \beta_i + M_i y \qquad (18)$$

$$J_i z = a_i . \sin \theta_i + b_i . \sin (\theta_i + \alpha_i) + M_i z$$
(19)

By applying trigonometric theorems, we obtain,

$$J_{ix} = (a_{i} \cdot \cos \theta_{i} + b_{i} (\cos \theta_{i} \cdot \cos \alpha_{i} - \sin \theta_{i} \cdot \sin \alpha_{i}))$$

$$\cos \beta_{i} + M_{ix}$$
(20)

$$J_{iy} = (a_i \cdot \cos \theta_i + b_i (\cos \theta_i \cdot \cos \alpha_i - \sin \theta_i \cdot \sin \alpha_i))$$

$$\sin \beta_i + M_{iy}$$
(21)

$$J_{iz} = (a_i . \sin \theta_i + b_i (\sin \theta_i . \cos \alpha_i + \cos \theta_i . \sin \alpha_i)) + M_{iz}$$
(22)

In this condition, the arm b_i remains perpendicular at 90° to the base, even when motor M_i moves. This is because point J_i is connected to the triangular plane above it, keeping arm b_i perpendicular. The simulation of this movement is shown in Figure 9. Based on this condition, the angle $\alpha_i = 90 + \theta_i$, so by applying the rules $\cos (90 + \theta_1) = -\sin \theta_i$ and $\sin (90 + \theta_1) = \cos \theta_i$, we obtain $\sin \alpha_i = \cos \theta_i$ and $\cos \alpha_i = -\sin \theta_i$. Then, by substituting in Eq. (20), Eq. (21), and Eq. (22), the following equations is derived.



FIGURE 9. Principle work of manipulator arm movement: (a) downward movement, (b) upward movement.

For the point x,

$$J_{i}x = (a_{i} \cos \theta_{i} + b_{i} (-\cos \theta_{i} \sin \theta_{i} - \sin \theta_{i} \cos \theta_{i})$$

$$\cos \beta_{i} + M_{i}x$$
(23)

$$J_i x = (a_i \cdot \cos \theta_i + b_i (-2 \sin \theta_i \cdot \cos \theta_i) \cos \beta_i + M_i x \quad (24)$$

$$J_i x = (a_i \cdot \cos \theta_i + b_i \cdot \sin 2\theta_i) \cdot \cos \beta_i + M_i x$$
(25)

For the point *y*,

$$J_{iy} = (a_i \cdot \cos \theta_i + b_i (-\cos \theta_i \cdot \sin \theta_i - \sin \theta_i \cdot \cos \theta_i)$$

$$\sin \beta_i + M_{iy}$$
(26)

$$J_i y = (a_i \cdot \cos \theta_i + b_i (-2 \sin \theta_i \cdot \cos \theta_i) \sin \beta_i + M_i y \quad (27)$$

$$J_i y = (a_i \cdot \cos \theta_i + b_i \cdot \sin 2\theta_i) \cdot \sin \beta_i + M_i y$$
(28)

For the point z,

$$J_{i}z = (a_{i}.\sin\theta_{i} + b_{i}(-\sin\theta_{i}.\sin\theta_{i} + \cos\theta_{i}.\cos\theta_{i}) + M_{i}z$$
(29)

$$J_{iz} = (a_i.\sin\theta_i + b_i\left(1 - 2\sin^2\theta_i\right) + M_{iz}$$
(30)

$$J_i z = a_i \cdot \sin \theta_i + b_i \cdot \cos 2\theta_i + M_i z \tag{31}$$

In the proposed system, the angle β_i varies for each motor. In Figure 10(a), the top view shows the orientation of motors M_1 , M_2 , and M_3 , each connected to arms a_1 , a_2 , and a_3 at points E_1 , E_2 , and E_3 . The angle between each motor is depicted, with 315° for M_1 , 45° for M_2 , and 180° for M_3 . Meanwhile, Figure 10(b) shows the physical layout or placement positions of the motors and the manipulator arms connected at the same points. These motors are strategically positioned to move each arm accurately.



FIGURE 10. The arrangement of servo motors from a top view: (a) orientation of each motor, (b) position of each motor.



FIGURE 11. The normal vector on the triangular plane.

Next, the tracker system's azimuth and altitude direction are calculated based on each motor's movement angle. To determine these values, it is necessary to calculate the normal vector of the triangular plane, as shown in Figure 11, where \vec{v}_0 is the initial normal vector when its direction is perpendicular upward, and \vec{v} is the normal vector when its direction changes. Based on the coordinate points $J_1(x_1, y_1, z_1)$, $J_2(x_2, y_2, z_2)$, and $J_3(x_3, y_3, z_3)$, the normal vector is calculated using the following equation,

$$\vec{v} = \vec{J_1 J_2} \cdot \vec{J_1 J_3} \tag{32}$$

where, $\overrightarrow{J_1J_2}$ is the vector from point J_1 to point J_2 and $\overrightarrow{J_1J_3}$ is the vector from point J_1 to point J_3 . The vectors in Eq. (32) can be calculated using the following equations,

$$\overline{J_1J_2} = (x_2 - x_1, y_2 - y_1, z_2 - z_1)$$
(33)

$$J_1 J_3 = (x_3 - x_1, y_3 - y_1, z_3 - z_1)$$
(34)

Thus, from Eq. (33) and Eq. (34), the normal vector is expressed as follows,

$$\vec{v} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ x_2 - x_1 & y_2 - y_1 & z_2 - z_1 \\ x_3 - x_1 & y_3 - y_1 & z_3 - z_1 \end{vmatrix}$$
(35)

So that, we obtain,

$$v_x = (y_2 - y_1) (z_3 - z_1) - (y_3 - y_1) (z_2 - z_1)$$
(36)

$$v_y = (x_2 - x_1) (z_3 - z_1) - (x_3 - x_1) (z_2 - z_1)$$
(37)

$$v_z = (x_2 - x_1) (y_3 - y_1) - (x_3 - x_1) (y_2 - y_1)$$
(38)

Based on Eq. (36), Eq. (37), and Eq. (38), the tilt angle of the plane concerning the *x*-axis (θ_x) and the *y*-axis (θ_y) can be determined using the following equations,

$$\theta_x = \cos^{-1}\left(\frac{v_x}{\sqrt{v_x^2 + v_y^2 + v_z^2}}\right)$$
(39)

$$\theta_y = \cos^{-1}\left(\frac{v_y}{\sqrt{v_x^2 + v_y^2 + v_z^2}}\right)$$
(40)

Meanwhile, to calculate the tracker azimuth (ϕ_T) and tracker altitude (φ_T) , the following equations are used,

$$\phi_T = \tan^{-1} \left(\frac{v_y}{v_x} \right) \tag{41}$$

$$\varphi_T = \tan^{-1} \left(\frac{v_z}{\sqrt{v_x^2 + v_y^2}} \right) \tag{42}$$

Meanwhile, point G is the centroid of the triangle and can be calculated using the following equation,

$$\begin{bmatrix} G_x \\ G_y \\ G_z \end{bmatrix} = \begin{bmatrix} (x_1 + x_2 + x_3)/3 \\ (y_1 + y_2 + y_3)/3 \\ (z_1 + z_2 + z_3)/3 \end{bmatrix}$$
(43)

IV. PERFORMANCE ANALYSIS

The analysis provides performance results of each model in predicting PV output power based on its operational temperature. The analytical methods used include calculating Mean Absolute Error (MAE), Root Mean Squared Error (RMSE), Mean Absolute Percentage Error (MAPE), Coefficient of Determination (R^2), and Coefficient of Variation (CV). MAE is one of the commonly used methods to analyze model performance. It measures the average absolute difference between the predicted values generated by the model and the actual values in the test data. This result shows how closely the model predictions match the actual values overall. The equation for MAE is as follows,

$$MAE = \frac{1}{n} \sum_{i=n}^{n} \left| y_i - \hat{y}_i \right| \tag{44}$$

where, *n* is the number of test data points, y_i is the actual value, and \hat{y}_i is the value predicted by the model for the *i* data point. A lower MAE value indicates better model performance, signifying that the model's predictions are closer to the actual values [66]. Next, RMSE analysis is conducted by calculating the square root of the average of the squared differences between the model's predicted values and the actual values. The equation for RMSE is defined as follows,

$$RMSE = \sqrt{\frac{1}{n} \sum_{i=n}^{n} (y_i - \hat{y}_i)^2}$$
(45)

RMSE analysis indicates the average deviation between the model's predicted and actual values. By taking the square root, RMSE offers a more intuitive interpretation in the same units as the target variable. A lower RMSE value indicates better model performance, meaning the model's predictions are closer to the actual values [67]. Next, MAPE analysis is a method to measure the error rate of a model by calculating the average of the absolute percentage error between the predicted and actual values. The equation for calculating MAPE is defined as follows,

$$MAPE = \frac{1}{n} \sum_{i=n}^{n} \left| \frac{y_i - \hat{y}_i}{y_i} \right| .100\%$$
(46)

The MAPE value indicates the prediction error in percentage terms. The lower the MAPE value, the better the model's performance in predicting the data. One advantage of MAPE is its ease of interpretation, as the result is a percentage. Next, the R^2 analysis, known as the Coefficient of Determination, is used to measure how well the developed model can explain the variability in the data. The equation for the Coefficient of Determination is defined as follows,

$$R^{2} = 1 - \frac{\sum_{i=1}^{n} (y_{i} - \hat{y}_{i})^{2}}{\sum_{i=1}^{n} (y_{i} - \hat{y})^{2}}$$
(47)

where, \hat{y} is the mean of all y_i values. The R^2 value ranges from 0 to 1, where a value closer to 1 indicates that the model better explains the variability in the data. R^2 analysis can determine how much output data variability can be explained by the input data. Lastly, the CV analysis, or Coefficient of Variation, is a statistical measure to assess a dataset's relative degree of variation. CV is defined as the ratio of the standard deviation to the mean, expressed as follows,

$$CV = \frac{\sqrt{\frac{1}{n}\sum_{i=1}^{n} \left(y_{i} - \frac{1}{n}\sum_{i=1}^{n} y_{i}\right)^{2}}}{\frac{1}{n}\sum_{i=1}^{n} y_{i}}$$
(48)

CV is typically used to measure data stability. A low CV value indicates more stable data, while a high CV value suggests more significant variability in the data.

V. RESULTS AND DISCUSSION

In this section, an evaluation is conducted to assess the performance of ANFIS in each model based on the type of consequent rule. Then, the movement of the three motors is simulated to obtain the azimuth and altitude angles. Testing uses the sun tracker device to assess the system's ability to track the sun's position. Finally, comparing previous systems is necessary to validate the proposed sun tracker system's effectiveness.

A. MODEL PERFORMANCE ANALYSIS

Table 4 presents the statistical results from the model's training and testing phases based on three types of consequent rules: first-order, second-order, and third-order. The dataset consists of 80% for training and 20% for testing. The ANFIS training and testing results show that the choice of consequent rule significantly impacts each model's performance.

In ANFIS model 1, the second-order performed best compared to the first-order and third-order, both in the training and testing phases. During training, the second-order achieved the lowest MAE, RMSE, and MAPE values, at 3.6, 4.5, and 8.08%, respectively, along with a high R^2 value of 0.98. This result indicates that the model can predict motor movement accurately based on the input data. In testing, the second-order also excelled with the lowest MAE, RMSE, and MAPE values, at 2.82, 3.34, and 7.02%, respectively, indicating accurate model performance with minimal error. In ANFIS model 2, a similar pattern emerged, with the second-order demonstrating optimal performance. During training, the second-order model yielded low MAE, RMSE, and MAPE values of 3.82, 4.74, and 8.3%, along with a high R^2 value of 0.97. In testing, the second-order produced MAE, RMSE, and MAPE values of 3, 3.58, and 6.44%, respectively, outperforming the first-order and third-order models. In ANFIS model 3, the second-order also provided the best results, achieving the lowest error values in training with MAE, RMSE, and MAPE of 3.8, 4.68, and 7.69%, respectively, and the highest R^2 value of 0.98. However, in testing, the second-order's performance was less optimal than the third-order, as indicated by higher MAE, RMSE, and MAPE values than the third-order. The training and testing analysis results show that the second-order consequent rule is optimal for all three ANFIS models.

Figure 12(a) displays the motor movement results with different consequent rules. The graph shows that all three consequent rules follow the angle change patterns quite well, although first-order shows more significant discrepancies.



FIGURE 12. The comparison analysis of consequence rule variations to controlling motor movements (a) ANFIS 1 model, (b) ANFIS 2 model, (c) ANFIS 3 model.

Meanwhile, in Figure 12(b), the first-order consequent rule exhibits noticeable differences, especially in the sixth and eighth experiments. On the other hand, second-order and third-order are more consistent in approaching the actual angle, although slight differences still exist at some points. In Figure 12(c), the average difference between the actual angle and the angle produced by each consequent rule is more minor than the previous graph. Overall, although both second-order and third-order consequent rules accurately follow the angle change patterns of all three motors, there are some points where the second-order performs better than the third-order. Figure 13 shows a three-dimensional graph illustrating the relationship between the ratio of two phototransistor values and the output as the motor angle increments for each consequent rule. The comparison values from the two phototransistor readings directly affect the magnitude of the resulting angle increment. In the first-order consequent, the angle increment pattern appears linear. In the second-order consequent, a significant angle increment occurs with more considerable phototransistor ratio differences; the greater the difference, the higher the angle increment. Conversely, there is no considerable angle increase for ratios closer in value. In the third-order, the angle increment pattern is similar to the second-order but displays fluctuations or a nonlinear pattern



FIGURE 13. The relationship between the phototransistor ratio values with the motor angle increases based on various consequent rules: (a) first-order, (b) second-order, and (c) third-order.

in the middle of the graph. This indicates that there are points where small changes in the phototransistor ratio can lead to a lower or even decreasing angle increment.

After obtaining the model, a motor movement simulation was conducted on the sun tracker to observe the relationship between the movements of the three motors and changes in azimuth and altitude angles. Figure 14 displays the simulation results, showing how each motor's activity influences the panel's orientation changes. In this simulation, it demonstrates the condition where the three motors move at angles



FIGURE 14. The simulation of azimuth and altitude changes based on motor movement ($M_1 = 26^\circ$, $M_2 = 40^\circ$, $M_3 = -30^\circ$).

 $M_1 = 26^\circ$, $M_1 = 40^\circ$, and $M_1 = -30^\circ$, resulting in a normal vector direction of (0, 8, 26) with tilt angles of $\theta_x =$ 90° and $\theta_y = 72^\circ$. Meanwhile, the resulting azimuth and altitude angles are 89° and 72° , respectively. Further testing results are shown in Figure 15, combining an angle range of -30° to 90° , representing the minimum to maximum motor angles. Figure 15(a) shows that the azimuth angle ranges from 0° to 360° , while Figure 15(b) indicates that the altitude angle ranges from 60° to 90° . This angle range demonstrates that the triple-axis mechanism can achieve good orientation flexibility, allowing the system to adjust the PV panel position effectively to minimize the solar incidence angle.

Subsequent testing was conducted to analyze the response of the sun tracker system in mitigating uncertain disturbances, such as the continuous movement of light due to cloud movement or shadows from external objects. The testing scenario involved observing the movement of the sun tracker at azimuth and altitude angles of 89° and 72°, respectively. The results of the sun tracker system's response based on ANFIS consequent rules are shown in Figure 16. Based on these tests, the proposed control rules were able to mitigate the effects of disturbances, such as changes in light intensity due to clouds, while maintaining the optimal orientation of the solar panel. Under partial shading conditions, where some sensors or PV panels receive reduced light intensity due to shadows from clouds or surrounding objects, the tracking system may face challenges in maintaining the optimal orientation of the solar panel toward the sun.

Further analysis was conducted to determine the system's response to each ANFIS consequent rule in response to changes in light position. The study was performed by comparing the system's response based on Figure 16. This analysis considered characteristics such as rise time, peak time, overshoot, settling time, and steady-state error for both

	D (Training		Testing			
Model	rarameter	First-Order	Second-Order	Third-Order	First-Order	Second-Order	Third-Order
	MAE	9.3	3.6	5.26	9.57	2.82	4.08
	RMSE	11.61	4.5	6.21	11.33	3.34	4.95
ANFIS 1	MAPE	21.79%	8.08%	17.08%	21.78%	7.02%	10.5%
	\mathbb{R}^2	0.81	0.98	0.96	0.83	0.99	0.97
	CV	0.39	0.49	0.47	0.42	0.47	0.44
	MAE	11.09	3.82	5.08	9.79	3	3.51
	RMSE	13.78	4.74	6.05	11.81	3.58	4.33
ANFIS 2	MAPE	19.44%	8.3%	12.86%	21.57%	6.44%	8.79%
	\mathbb{R}^2	0.69	0.97	0.95	0.82	0.99	0.98
	CV	0.3	0.42	0.4	0.4	0.46	0.46
	MAE	11.76	3.8	4.41	8.94	2.86	2.77
	RMSE	14.1	4.68	5.33	10.86	3.48	3.4
ANFIS 3	MAPE	22.83%	7.69%	8.83%	18.52%	6.35%	6.11%
	R ²	0.7	0.98	0.97	0.85	0.99	0.99
	CV	0.35	0.48	0.43	0.41	0.47	0.47

TABLE 4. The results of ANFIS training and testing with various consequent rules.



FIGURE 15. The results of the sun tracker movement experiment based on all combinations of angles M_1, M_2 , and M_3 : (a) azimuth angle movement and (b) altitude angle movement.



FIGURE 16. The comparison result of responses to light changes for each ANFISconsequent rules (a) azimuth movement, (b) altitude movement.

azimuth and altitude movements, which are presented in Table 5 and Table 6. For azimuth movement, second-order showed the most optimal performance, achieving the fastest



first-order. In the first-order, the settling time was unavailable because the system response did not reach a steady-state condition during the observation period. For altitude movement, the analysis also indicated that the second-order performed better than the others. No overshoot occurred in the secondorder, as with the azimuth movement. In the first-order, the settling time was also unavailable, as the system response did not reach a steady-state condition. This analysis reveals that second-order is the best choice for controlling both azimuth and altitude movements, making this consequent rule most suitable for implementation in ANFIS-PCT for a triple-axis sun tracker system.

 TABLE 5. The comparison of performance ANFIS consequent rules on azimuth movement.

Parameter	First-order	Second-order	Third-order
Rise Time (s)	0.681	0.601	0.661
Peak Time (s)	1.403	1.723	1.483
Overshoot (%)	0.899	0	0.562
Settling Time (s)	-	1.462	2.212
Steady State Error	0.679	0.03	0.111

 TABLE 6. The comparison of performance ANFIS consequent rules on altitude movement.

Parameter	First-order	Second-order	Third-order
Rise Time (s)	0.511	0.491	0.521
Peak Time (s)	2.685	1.493	1.283
Overshoot (%)	0.556	0	0.139
Settling Time (s)	-	1.34	1.538
Steady State Error	0.399	0.027	0.213

B. SUN TRACKER SYSTEM PERFORMANCE ANALYSIS

Figure 17(a) compares the sun tracker movement and the azimuth angle of the actual sun position. The graph shows the sun tracker accurately follows the sun's azimuth angle from sunrise to sunset. Meanwhile, Figure 17(b) compares the altitude angle. Based on this graph, a discrepancy occurs at the start of tracking, around 7:00 AM to 8:00 AM. Then, the sun tracker successfully tracks the sun's altitude more accurately, reaching a peak at 12:30 PM at its maximum altitude. Afterwards, the altitude of the sun tracker gradually decreases in sync with the sun's position until sunset. Overall, the sun tracker system works effectively to adjust its movement in tracking the sun's position in azimuth and altitude angles, thereby minimizing the solar incidence angle on the PV surface throughout the day.

C. SYSTEM PERFORMANCE COMPARISON

Table 7 compares the proposed ANFIS model's performance with several previous models related to sun tracker systems. The comparison aims to validate the performance of the proposed ANFIS model in tracking the sun's position. The models compared include PID-ANN [44], Fast Integral



FIGURE 17. The result comparison between the tracked and the sun's actual position: (a) azimuth movement and (b) altitude movement.

Terminal Sliding Mode Control (FIT-SMC) [68], Neural Network Algorithm with Model Predictive Control (NNA-MPC) [69], PID with Internal Model Controller (PID-IMC) [51], PID with Fuzzy Logic Controller (PID-FLC) [48], PD with Fuzzy Logic Controller (PD-FLC) [46], and Artificial Bee Colony (ABC) [50]. The parameters compared are rise time, settling time, and steady-state error. Based on the comparison, the proposed ANFIS-PCT model demonstrates optimal performance. For the rise time parameter, ANFIS-PCT has a relatively fast time, only behind the FIT-SMC model, which recorded the most rapid rise time of 0.15 seconds. However, compared to other models, ANFIS-PCT is far superior. For the settling time parameter, ANFIS-PCT also shows optimal performance, although it is still behind FIT-SMC, which recorded the fastest time. Meanwhile, for the steady-state error, ANFIS-PCT demonstrates a more stable and accurate system.

 TABLE 7. The comparison of the proposed ANFIS model with other published models.

Model	Rise Time (s)	Settling Time (s)	Steady State Error
ANFIS-PCT (Proposed)	0.55	1.4	0.03
PID-ANN	2.18	2.46	0.07
FIT-SMC	0.15	0.33	-
NNA-MPC	-	0.108	-
PID-IMC	1.8	5.58	-
PID-FLC	3.6	4.8	0.4
PD-FLC	6.38	6.38	0.83
ABC	2.37	5.23	1.05

VI. CONCLUSION

Based on the analysis results, all three proposed ANFIS models using the second-order consequent rule deliver the

best performance compared to the first-order and third-order, both in the training and testing phases. The simulation results show that the movement of the sun tracker with a triple-axis mechanism can reach an azimuth angle ranging from 0° to 360° . In contrast, the altitude angle ranges from 60° to 90° . These values indicate that the sun tracker has good flexibility. The proposed system has nonlinear dynamics, so several parameters must be continuously optimized through the training process to gradually reduce the error value in the system until it approaches zero. This indicates that the system will always move towards stability, even with small variations in input parameters or disturbances.

Although the proposed sun tracker system offers improved accuracy and responsiveness in tracking the sun's position, it has some drawbacks, including system complexity, leading to higher energy consumption. This is due to the number of motors that need to move simultaneously to reach the optimal position. The additional energy the motors consume in the triple-axis mechanism can reduce overall energy efficiency, especially in conditions with limited energy sources.

Future research will focus on developing triple-axis sun tracker technology techniques to enhance efficiency by reducing energy consumption and optimizing PCT in ANFIS to make it more adaptive in tracking the sun's position. Further research can be developed by exploring the Lyapunov method to explicitly determine the stability of the sun tracker system, allowing the mathematical proof to support the experimental results that have been conducted. Additionally, future research will focus on exploring energy-saving strategies, including optimizing by reducing unnecessary servo motor movements, as well as evaluating the comparison between the energy produced and the total energy consumed.

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